

Results of Proficiency Test
Engine Oil (fresh)
June 2020

Organized by: Institute for Interlaboratory Studies
Spijkenisse, the Netherlands

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Report: iis20L06 == Revised ==

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SUMMARY OF CHANGES

This revised report replaces the original report iis20L06 of September 2020.

It was discovered that accidentally a wrong test value was excluded in the evaluation of the Viscosity Index (appendix 1). In the original report iis20L06 test value 142.09 submitted by lab 254 was excluded for having an outlier in Kinematic Viscosity 40°C. This should have been test value 146 submitted by lab 237. Regretfully, this mistake has impact on the mean value and therefore on the calculated z-scores. It is therefore decided to publish a revised report iis20L06-revised in which this mistake has been corrected.

The following in this report has been revised:

- Viscosity Index mean value and calculated R ($2.8 * sd$) in paragraph 4.2, table 3
- The calculated z-scores, statistical details and pictures of Viscosity Index in appendix 1 on pages 44 and 45 (pages 42 and 43 of the original report)

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1 INTRODUCTION

Since 1997 a proficiency test for fresh Engine Oil (Lubricating Oil) is organized by the Institute for Interlaboratory Studies every year. During the annual proficiency testing program 2019/2020 it was decided to continue the round robin for the analysis of Engine Oil (fresh) in accordance with the latest version of ASTM D4485 and ACEA European Oil Sequences.

In this interlaboratory study 73 laboratories in 44 countries registered for participation. See appendix 2 for the number of participants per country. In this report the results of this proficiency test for Engine Oil (fresh) are presented and discussed. This report is also electronically available through the iis website www.iisnl.com.

2 SET UP

The Institute for Interlaboratory Studies (iis) in Spijkenisse, the Netherlands, was the organizer of this proficiency test (PT). Sample analyzes for fit-for-use and homogeneity testing were subcontracted to an ISO/IEC17025 accredited laboratory. It was decided to send to each laboratory one 1L bottle and one 0.5L bottle of the same Engine Oil (fresh), both labelled #20075. The participants were requested to report rounded and unrounded test results. The unrounded test results were preferably used for statistical evaluation.

2.1 ACCREDITATION

The Institute for Interlaboratory Studies in Spijkenisse, the Netherlands, is accredited in agreement with ISO/IEC17043:2010 (R007), since January 2000, by the Dutch Accreditation Council (Raad voor Accreditatie). This PT falls under the accredited scope. This ensures strict adherence to protocols for sample preparation and statistical evaluation and 100% confidentiality of participant's data. Feedback from the participants on the reported data is encouraged and customer's satisfaction is measured on regular basis by sending out questionnaires.

2.2 PROTOCOL

The protocol followed in the organization was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of June 2018 (iis-protocol, version 3.5). This protocol is electronically available through the iis website www.iisnl.com, from the FAQ page.

2.3 CONFIDENTIALITY STATEMENT

All data presented in this report must be regarded as confidential and for use by the participating companies only. Disclosure of the information in this report is only allowed by means of the entire report. Use of the contents of this report for third parties is only allowed by written permission of the Institute for Interlaboratory Studies. Disclosure of the identity of one or more of the participating companies will be done only after receipt of a written agreement of the companies involved.

2.4 SAMPLES

A batch of approximately 200 liters of an 10W-30 Diesel Engine Oil was obtained from a local supplier. After homogenization 108 amber glass bottles of 1L and 108 amber glass bottles of 0.5L were filled and both labelled #20075.

The homogeneity of the subsamples was checked by determination of Density in accordance with ISO12185 on 8 stratified randomly selected subsamples.

| | Density at 15°C in kg/L |
|-----------------|----------------------------|
| Sample #20075-1 | 0.86751 |
| Sample #20075-2 | 0.86751 |
| Sample #20075-3 | 0.86751 |
| Sample #20075-4 | 0.86750 |
| Sample #20075-5 | 0.86751 |
| Sample #20075-6 | 0.86750 |
| Sample #20075-7 | 0.86751 |
| Sample #20075-8 | 0.86751 |

Table 1: homogeneity test results of subsamples #20075

From the above test results the repeatability was calculated and compared with 0.3 times the reproducibility of the reference test method in agreement with the procedure of ISO13528, Annex B2 in the next table.

| | Density at 15°C in kg/L |
|---------------------------------|----------------------------|
| r (observed) | 0.00001 |
| reference test method | ISO12185:96 |
| 0.3 * R (reference test method) | 0.00015 |

Table 2: evaluation of the repeatability of the subsamples #20075

The calculated repeatability was less than 0.3 times the reproducibility of the reference test method. Therefore, homogeneity of the subsamples was assumed.

To each of the participating laboratories one bottle of 1 liter and one bottle of 0.5 liter of Engine Oil (fresh) both labelled #20075 were sent on May 13, 2020. An SDS was added to the sample package.

2.5 STABILITY OF THE SAMPLES

The stability of the fresh Engine Oil packed in amber glass bottles was checked. The material was found sufficiently stable for the period of the proficiency test.

2.6 ANALYZES

The participants were requested to determine on sample #20075: Total Acid Number, Base Number (HClO₄ titration), Color ASTM, Conradson Carbon Residue, Ramsbottom Carbon Residue, Carbon Residue (micro method), Density at 15°C, Evaporation loss by Noack, Flash Point C.O.C., Flash Point PMcc, Foaming Tendency, Foam Stability, Kinematic Viscosity (40°C and 100°C), Viscosity Index, Viscosity Stabinger (40°C and 100°C), Viscosity Apparent (CCS) at -25°C, Viscosity HTHS, Nitrogen, Pour Point (Manual and Automated), Sulfated Ash, Sulfur, Water, Calcium, Phosphorus and Zinc. Some additional questions were asked about Total Acid Number and Foaming Characteristics.

It was explicitly requested to treat the samples as if they were routine samples and to report the test results using the indicated units on the report form and not to round the test results, but report as much significant figures as possible. It was also requested not to report 'less than' test results, which are above the detection limit, because such test results cannot be used for meaningful statistical evaluations.

To get comparable test results, a detailed report form and a letter of instructions are prepared. On the report form, the reporting units are given as well as the reference test methods that will be used during the evaluation. The detailed report form and the letter of instructions are both made available on the data entry portal www.kpmd.co.uk/sgs-iis/. The participating laboratories are also requested to confirm the sample receipt on this data entry portal. The letter of instructions can also be downloaded from the iis website www.iisnl.com.

3 RESULTS

During five weeks after sample dispatch, the test results of the individual laboratories were gathered via the data entry portal www.kpmd.co.uk/sgs-iis/. The reported test results are tabulated per determination in appendix 1 of this report. The laboratories are presented by their code numbers.

Directly after the deadline a reminder was sent to those laboratories that had not reported test results at that moment. Shortly after the deadline the available test results were screened for suspect data. A test result was called suspect in case the Huber Elimination Rule (a robust outlier test) found it to be an outlier. The laboratories that produced these suspect data were asked to check the reported test results (no reanalyzes). Additional or corrected test results are used for data analysis and reported test results are placed under 'Remarks' in the test result tables in appendix 1. Test results that came in after the deadline were not taken into account in this screening for suspect data and thus these participants were not requested for checks.

3.1 STATISTICS

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of June 2018 (iis-protocol, version 3.5).

For the statistical evaluation the *unrounded* (when available) figures were used instead of the rounded test results. Test results reported as '<...' or '>...' were not used in the statistical evaluation.

First, the normality of the distribution of the various data sets per determination was checked by means of the Lilliefors-test, a variant of the Kolmogorov-Smirnov test and by the calculation of skewness and kurtosis. Evaluation of the three normality indicators in combination with the visual evaluation of the graphic Kernel density plot, lead to judgement of the normality being either 'unknown', 'OK', 'suspect' or 'not OK'. After removal of outliers, this check was repeated. If a data set does not have a normal distribution, the (results of the) statistical evaluation should be used with due care.

According to ISO5725 the reported test results per determination were submitted to Dixon's, Grubbs' and/or Rosner's outlier tests. Outliers are marked by D(0.01) for the Dixon's test, by G(0.01) or DG(0.01) for the Grubbs' test and by R(0.01) for the Rosner's test. Stragglers are marked by D(0.05) for the Dixon's test, by G(0.05) or DG(0.05) for the Grubbs' test and by R(0.05) for the Rosner's test. Both outliers and stragglers were not included in the calculations of averages and standard deviations.

For each assigned value the uncertainty was determined in accordance with ISO13528. Subsequently the calculated uncertainty was evaluated against the respective requirement based on the target reproducibility in accordance with ISO13528. In this PT, the criterion of ISO13528, paragraph 9.2.1. was met for all evaluated tests, therefore, the uncertainty of all assigned values may be negligible and need not be included in the PT report.

Finally, the reproducibilities were calculated from the standard deviations by multiplying them with a factor of 2.8.

3.2 GRAPHICS

In order to visualize the data against the reproducibilities from literature, Gauss plots were made, using the sorted data for one determination (see appendix 1). On the Y-axis the reported test results are plotted. The corresponding laboratory numbers are on the X-axis. The straight horizontal line presents the consensus value (a trimmed mean). The four striped lines, parallel to the consensus value line, are the +3s, +2s, -2s and -3s target reproducibility limits of the selected reference test method. Outliers and other data, which were excluded from the calculations, are represented as a cross. Accepted data are represented as a triangle. Furthermore, Kernel Density Graphs were made. This is a method for producing a smooth density approximation to a set of data that avoids some problems associated with histograms. Also, a normal Gauss curve was projected over the Kernel Density Graph for reference.

3.3 Z-SCORES

To evaluate the performance of the participating laboratories the z-scores were calculated. As it was decided to evaluate the performance of the participants in this proficiency test (PT) against the literature requirements, e.g. ASTM or ISO reproducibilities, the z-scores were calculated using a target standard deviation. This results in an evaluation independent of the variation of this interlaboratory study.

The target standard deviation was calculated from the literature reproducibility by division with 2.8. In case no literature reproducibility was available, other target values were used. In some cases, a reproducibility based on former iis proficiency tests could be used. When a laboratory did use a test method with a reproducibility that is significantly different from the reproducibility of the reference test method used in this report, it is strongly advised to recalculate the z-score, while using the reproducibility of the actual test method used, this in order to evaluate whether the reported test result is fit-for-use.

The z-scores were calculated according to:

$$Z_{(\text{target})} = (\text{test result} - \text{average of PT}) / \text{target standard deviation}$$

The $Z_{(\text{target})}$ scores are listed in the test result tables in appendix 1.

Absolute values for $z < 2$ are very common and absolute values for $z > 3$ are very rare. The usual interpretation of z-scores is as follows:

| | |
|---------------|----------------|
| $ z < 1$ | good |
| $1 < z < 2$ | satisfactory |
| $2 < z < 3$ | questionable |
| $3 < z $ | unsatisfactory |

4 EVALUATION

In this interlaboratory study some problems were encountered with the dispatch of the samples due to the COVID-19 pandemic. Therefore, the reporting time on the data entry portal was extended with another three weeks. After this period still eleven participants did not report any test results. Not all participants were able to report test results for all requested tests.

In total 62 participants reported 961 numerical test results. Observed were 34 outlying test results, which is 3.5%. In proficiency studies, outlier percentages of 3% - 7.5% are quite normal.

Not all original data sets proved to have a normal Gaussian distribution. These are referred to as “not OK” or “suspect”. The statistical evaluation of these data sets should be used with due care, see also paragraph 3.1.

4.1 EVALUATION PER TEST

In this section the reported test results are discussed per test. The test methods, which are used by the various laboratories, are taken into account for explaining the observed differences when possible and applicable. These test methods are also in the tables together with the reported test results. The abbreviations, used in these tables, are explained in appendix 3.

In the iis PT reports ASTM methods are referred to with a number (e.g. D1500) and an added designation for the year that the method was adopted or revised (e.g. D1500:12). If applicable, a designation in parentheses is added to designate the year of reapproval (e.g. D1500:12 (2017)). In the results tables of appendix 1 only the method number and year of adoption or revision (e.g. D1500:12) will be used.

Total Acid Number: This determination was very problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not at all in agreement with the requirements of ASTM D664-A:18e2 regardless of which type of end point determination was used (Buffer End Point or Inflection Point) and what volume of titration solvent was used (60 mL or 125 mL).
When evaluated separately for the type of end point the calculated reproducibility of the group using Inflection Point (IP) was still not in agreement with the requirements of inflection point at both titration volumes from test method D664-A:18e2. The calculated reproducibility of the group using BEP (pH 10 and 11) is still not in agreement with the requirements of BEP (pH 10) from test method D664-A:18e2 for 60 mL and 125 mL. It is observed that seven participants reported to have used pH 11 for BEP. Please note that in method ASTM D664-A version 2018e2 the Buffer End Point has been changed to pH 10. Furthermore, it is remarkable that BEP has been used for a fresh oil. Test method ASTM D664-A advises to use BEP for used oils.

Base Number (HClO₄ titration): This determination was not problematic. Five statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of the forward mode of ASTM D2896-A:15.

Color ASTM: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D1500:12(2017). Please note: the test values reported as "text" were converted to a numerical value before calculating the z-scores (e.g. L3.5 to 3.25, see also appendix 1).

Conradson Carbon Residue: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ASTM D189:06(2014).

Ramsbottom Carbon Residue: Only two participants reported a test result. Therefore, no z-scores were calculated.

Carbon Residue (micro method): This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D4530:15.

Density at 15°C: This determination was not problematic. Four statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ISO12185:96.

Evaporation loss by Noack: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D5800:19a for procedure B and procedure A. When evaluated separately for the test results of procedure A and B from ASTM D5800 the calculated reproducibility is also in agreement with the requirements of both procedures from ASTM D5800:19a.

Flash Point C.O.C.: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is full in agreement with the requirements of ASTM D92:18.

Flash Point PMcc: This determination was not problematic. Four statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D93-A:19.

Foaming Tendency: This determination may be problematic dependent on the sequence reported. In total three statistical outliers were observed. The calculated reproducibility after rejection of the statistical outlier for Sequence III is in agreement with the requirements of ASTM D892:13e1. The calculated reproducibilities of Sequence I and II are not in agreement with the requirements of ASTM D892:13e1. When evaluated separately for the two type of diffusers a difference in mean values between stone and metal diffusers was observed for Sequence I and II (see appendix 1). The group that used a stone diffuser for Sequence I meets the requirements of method ASTM D892:13e1. A new version of method ASTM D892 was published in 2018. In this version, the precision data has been "changed". In the 2018 version exponential equations were published for Sequence I and III and a linear equation for Sequence II. After investigation, the 2018 reproducibility equations are based on the same underlying round robin data as the precision chart figure 4 of ASTM D892:13e1. However, the equations of sequence I and III are given as exponential equations without an intercept. The consequences for low Foam values (0 - 10 mL) are that the new exponential equations will result in a reproducibility between 0 and 7 mL, while the 2013 linear plots result in a reproducibility of 15 to 16 mL. The 2018 linear equation published for Sequence II is comparable to the linear plot of 2013. Taking all this into account, it is decided for this PT to use the less strict and more realistic precision data of version 2013 to calculate the z-scores. The precision data of the 2018 version are given as reference.

Foam Stability: All reporting participants agreed on a result of 0 (Nil). Therefore, no z-scores were calculated.

Kinematic Viscosity at 40°C: This determination was not problematic. Four statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D445:19.

Kinematic Viscosity at 100°C: This determination was not problematic. Two statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D445:19.

Viscosity Index: This determination was problematic. No statistical outliers were observed but six test results were excluded. The calculated reproducibility after rejection of the suspect data is not in agreement with the requirements of ASTM D2270:10(2016).

Viscosity Stabinger at 40°C: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in full agreement with the requirements of ASTM D7042:19e1.

Viscosity Stabinger at 100°C: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements ASTM D7042:19e1.

Viscosity Apparent (CCS) at -25°C: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D5293:17a.

Viscosity HTHS: This determination was problematic. No statistical outliers were observed. However, the calculated reproducibility is not in agreement with the requirements of ASTM D4683:17.

Nitrogen: This determination was problematic. No statistical outliers were observed. However, the calculated reproducibility is not in agreement with the requirements of ASTM D5762:18a. A possible cause could be that combustion tube temperatures are not adjusted/verified well enough, which can lead to lower temperatures and a low yield.

Pour Point Manual: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in full agreement with the requirements of ASTM D97:17b.

Pour Point Automated: This determination was very problematic. No statistical outliers were observed. However, the calculated reproducibility is not at all in agreement with the requirements of ASTM D5950:14.

Sulfated Ash: This determination was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is in full agreement with the requirements of ASTM D874:13a(2018).

Sulfur: This determination was problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not in agreement with the requirements of ASTM D4294:16e1.

Water: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D6304:16e1.

Calcium: This determination was problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is not in agreement with the requirements of ASTM D5185:18.

Phosphorus: This determination was problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is not in agreement with the requirements of ASTM D5185:18.

Zinc: This determination was not problematic. Three statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D5185:18.

4.2 PERFORMANCE EVALUATION FOR THE GROUP OF LABORATORIES

A comparison has been made between the reproducibility as declared by the reference test method and the reproducibility as found for the group of participating laboratories. The number of significant test results, the average, the calculated reproducibility (2.8 * standard deviation) and the target reproducibility derived from the literature reference test methods (in casu ASTM, ISO test methods) are presented in the next table.

| Parameter | unit | n | average | 2.8 * sd | R(lit) |
|---|----------|----|---------|----------|--------|
| Total Acid Number | mg KOH/g | 37 | 2.00 | 1.65 | 0.71 |
| Base Number (HClO ₄ titration) | mg KOH/g | 36 | 9.7 | 0.6 | 0.7 |
| Color ASTM | | 48 | 3.5 | 0.6 | 1 |
| Conradson Carbon Residue | %M/M | 15 | 1.01 | 0.19 | 0.24 |
| Ramsbottom Carbon Residue | %M/M | 2 | <1 | n.e. | n.e. |
| Carbon Residue (micro method) | %M/M | 20 | 1.03 | 0.13 | 0.19 |
| Density at 15°C | kg/L | 49 | 0.8675 | 0.0004 | 0.0005 |
| Evaporation loss by Noack | %M/M | 16 | 10.71 | 1.20 | 1.41 |
| Flash Point C.O.C. | °C | 44 | 229.7 | 18.1 | 18 |
| Flash Point PMcc | °C | 40 | 198.9 | 8.6 | 14.1 |
| Foaming Tendency, Sequence I | mL | 27 | 7.4 | 22.1 | 17.2 |
| Foaming Tendency, Sequence II | mL | 27 | 29.3 | 44.2 | 26.8 |
| Foaming Tendency, Sequence III | mL | 25 | 4.0 | 13.4 | 15.7 |
| Foam Stability, Sequence I | mL | 26 | 0 | n.a. | n.a. |
| Foam Stability, Sequence II | mL | 27 | 0 | n.a. | n.a. |

| Parameter | unit | n | average | 2.8 * sd | R(lit) |
|--------------------------------|--------------------|----|---------|----------|--------|
| Foam Stability, Sequence III | mL | 26 | 0 | n.a. | n.a. |
| Kinematic Viscosity at 40°C | mm ² /s | 50 | 79.39 | 0.53 | 0.97 |
| Kinematic Viscosity at 100°C | mm ² /s | 51 | 11.77 | 0.13 | 0.16 |
| Viscosity Index | | 47 | 141.8 | 2.6 | 2 |
| Viscosity Stabinger at 40°C | mm ² /s | 19 | 79.57 | 0.98 | 0.98 |
| Viscosity Stabinger at 100°C | mm ² /s | 18 | 11.79 | 0.09 | 0.12 |
| Viscosity Apparent (CCS) -25°C | mPa·s | 19 | 6601 | 344 | 482 |
| Viscosity HTHS | mPa·s | 4 | 3.56 | 0.20 | 0.15 |
| Nitrogen | mg/kg | 15 | 1310 | 531 | 349 |
| Pour Point Manual | °C | 26 | -38.8 | 9.1 | 9 |
| Pour Point Automated 1°C int. | °C | 17 | -42.1 | 9.1 | 4.5 |
| Sulfated Ash | %M/M | 31 | 0.92 | 0.13 | 0.13 |
| Sulfur | mg/kg | 29 | 2167 | 388 | 271 |
| Water | mg/kg | 32 | 190 | 247 | 394 |
| Calcium as Ca | mg/kg | 38 | 1587 | 290 | 217 |
| Phosphorus as P | mg/kg | 36 | 777 | 133 | 120 |
| Zinc as Zn | mg/kg | 36 | 882 | 121 | 144 |

Table 3: reproducibilities of tests on sample #20075

Without further statistical calculations it can be concluded that for most tests there is a good compliance of the group of participants with the reference test methods. The tests that are problematic have been discussed in paragraph 4.1.

4.3 COMPARISON OF THE PROFICIENCY TEST OF JUNE 2020 WITH PREVIOUS PTS

| | June 2020 | June 2019 | June 2018 | June 2017 | June 2016 |
|------------------------------------|-----------|-----------|-----------|-----------|-----------|
| Number of reporting laboratories | 62 | 75 | 81 | 67 | 69 |
| Number of test results | 961 | 1157 | 1337 | 940 | 1007 |
| Number of statistical outliers | 34 | 49 | 37 | 45 | 25 |
| Percentage of statistical outliers | 3.5% | 4.2% | 2.8% | 4.8% | 2.5% |

Table 4: comparison with previous proficiency tests

In proficiency tests, outlier percentages of 3% - 7.5% are quite normal.

The performance of the determinations of the proficiency tests was compared against the requirements of the respective reference test methods. The conclusions are given in the following table.

| Determination | June 2020 | June 2019 | June 2018 | June 2017 | June 2016 |
|---|-----------|-----------|-----------|-----------|-----------|
| Total Acid Number | -- | -- | - | -- | -- |
| Base Number (HClO ₄ titration) | + | + | - | - | - |
| Color ASTM | + | + | + | - | + |
| Conradson Carbon Residue | + | + | +/- | + | + |
| Ramsbottom Carbon Residue | n.e. | (--) | + | + | -- |
| Carbon Residue (micro method) | + | - | + | +/- | + |
| Density at 15°C | + | +/- | +/- | + | + |
| Evaporation loss by Noack | + | -- | - | + | - |
| Flash Point C.O.C. | +/- | +/- | + | - | + |
| Flash Point PMcc | + | + | + | +/- | + |
| Foaming Tendency | - | +/- | +/- | +/- | +/- |
| Kinematic Viscosity at 40°C | + | + | + | + | +/- |
| Kinematic Viscosity at 100°C | + | +/- | + | + | + |
| Viscosity Index | - | - | +/- | +/- | - |
| Viscosity Stabinger at 40°C | +/- | +/- | +/- | - | - |
| Viscosity Stabinger at 100°C | + | +/- | - | - | - |
| Viscosity Apparent (CCS) -25°C | + | + | - | +/- | + |
| Viscosity HTHS | - | +/- | + | + | + |
| Nitrogen | - | -- | - | - | - |
| Pour Point Manual | +/- | + | +/- | - | + |
| Pour Point Automated 1°C int. | -- | + | +/- | - | - |
| Sulfated Ash | +/- | - | - | + | - |
| Sulfur | - | (--) | - | - | - |
| Water | + | + | + | +/- | + |
| Calcium as Ca | - | + | - | + | -- |
| Phosphorus as P | - | - | - | n.e. | -- |
| Zinc as Zn | + | +/- | +/- | n.e. | -- |

Table 5: comparison determinations against the reference test methods

For evaluations between brackets no z-scores are calculated

The following performance categories were used:

- ++ : group performed much better than the reference test method
- + : group performed better than the reference test method
- +/- : group performance equals the reference test method
- : group performed worse than the reference test method
- : group performed much worse than the reference test method
- n.e. : not evaluated

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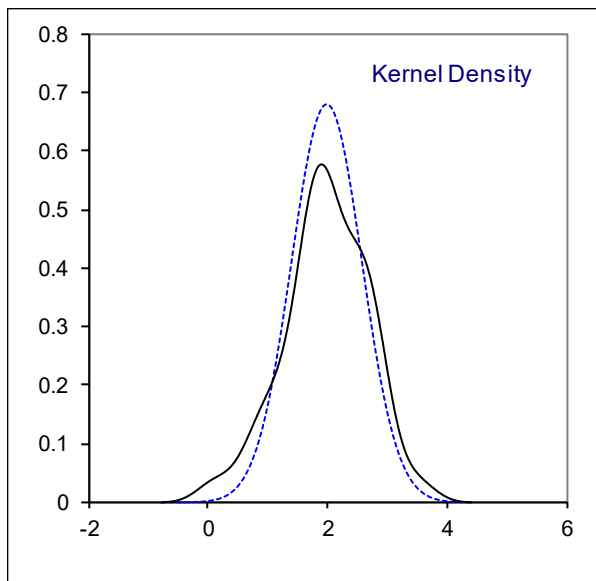
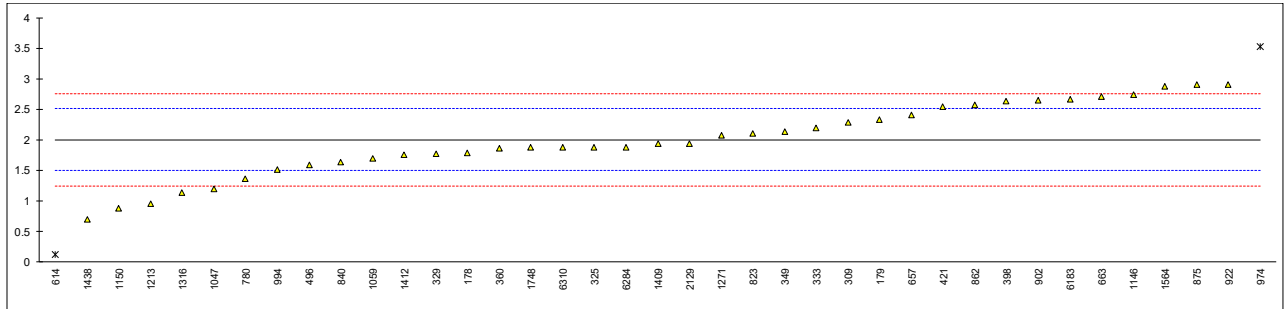
APPENDIX 1

Determination of Total Acid Number on sample #20075; results in mg KOH/g

| lab | method | value | mark | z(targ) | end point determination | titration solvent volume |
|------|----------|--------|---------|---------|--------------------------|--------------------------|
| 178 | D664-A | 1.78 | | -0.86 | Buffer End Point (pH 11) | 60 mL |
| 179 | D664-A | 2.33 | | 1.31 | Inflection Point | 60 mL |
| 211 | | ---- | | ---- | --- | --- |
| 219 | | ---- | | ---- | --- | --- |
| 237 | | ---- | | ---- | --- | --- |
| 254 | | ---- | | ---- | --- | --- |
| 255 | | ---- | | ---- | --- | --- |
| 257 | | ---- | | ---- | --- | --- |
| 309 | D664-A | 2.29 | | 1.15 | Buffer End Point (pH 10) | 60 mL |
| 325 | D664-A | 1.88 | | -0.47 | Buffer End Point (pH 10) | 125 mL |
| 329 | D664-A | 1.77 | | -0.90 | Inflection Point | 125 mL |
| 333 | D664-A | 2.2 | | 0.79 | Inflection Point | 125 mL |
| 339 | | ---- | | ---- | --- | --- |
| 349 | D664-A | 2.14 | | 0.56 | Inflection Point | 125 mL |
| 360 | D664-A | 1.866 | | -0.52 | Inflection Point | 60 mL |
| 398 | D664-A | 2.625 | | 2.47 | Inflection Point | 60 mL |
| 421 | ISO6619 | 2.54 | | 2.14 | --- | --- |
| 432 | | ---- | | ---- | --- | --- |
| 496 | D664-A | 1.59 | | -1.61 | Buffer End Point (pH 10) | 60 mL |
| 614 | D664-A | 0.13 | R(0.01) | -7.37 | --- | 60 mL |
| 621 | | ---- | | ---- | --- | --- |
| 633 | | ---- | | ---- | --- | --- |
| 634 | | ---- | | ---- | --- | --- |
| 657 | D664-A | 2.41 | C | 1.62 | Inflection Point | 125 mL |
| 663 | D664-A | 2.709 | | 2.80 | Buffer End Point (pH 10) | 60 mL |
| 780 | D664-A | 1.37 | | -2.48 | Buffer End Point (pH 10) | 125 mL |
| 823 | D664-A | 2.1 | | 0.40 | Inflection Point | 125 mL |
| 840 | D664-B | 1.64 | | -1.42 | Buffer End Point (pH 10) | 60 mL |
| 862 | D664-A | 2.57 | | 2.25 | Inflection Point | 60 mL |
| 875 | D664-A | 2.90 | | 3.56 | --- | --- |
| 902 | D664-A | 2.653 | | 2.58 | Inflection Point | 60 mL |
| 912 | | ---- | | ---- | --- | --- |
| 913 | | ---- | | ---- | --- | --- |
| 922 | D664-A | 2.9 | | 3.56 | Inflection Point | 125 mL |
| 962 | | ---- | | ---- | --- | --- |
| 963 | | ---- | | ---- | --- | --- |
| 974 | D664-A | 3.52 | R(0.01) | 6.00 | Inflection Point | 125 mL |
| 994 | D664-A | 1.52 | | -1.89 | Buffer End Point (pH 11) | 60 mL |
| 1011 | | ---- | | ---- | --- | --- |
| 1017 | | ---- | | ---- | --- | --- |
| 1047 | ISO6618 | 1.2 | | -3.15 | --- | 60 mL |
| 1059 | ISO6619 | 1.70 | | -1.18 | Buffer End Point (pH 11) | 60 mL |
| 1091 | | ---- | | ---- | --- | --- |
| 1146 | D664-A | 2.733 | | 2.90 | Buffer End Point (pH 11) | 125 mL |
| 1150 | In house | 0.8838 | | -4.40 | --- | --- |
| 1173 | | ---- | | ---- | --- | --- |
| 1213 | D664-A | 0.95 | | -4.14 | --- | --- |
| 1235 | | ---- | | ---- | --- | --- |
| 1271 | D664-A | 2.08 | | 0.32 | Inflection Point | 125 mL |
| 1316 | D664-A | 1.14 | | -3.39 | Buffer End Point (pH 11) | 60 mL |
| 1320 | | ---- | | ---- | --- | --- |
| 1409 | D664-A | 1.93 | | -0.27 | Buffer End Point (pH 11) | 60 mL |
| 1412 | D664-A | 1.76 | | -0.94 | Buffer End Point (pH 11) | 125 mL |
| 1438 | | 0.697 | | -5.14 | --- | --- |
| 1461 | | ---- | | ---- | --- | --- |
| 1510 | | ---- | | ---- | --- | --- |
| 1564 | D664-A | 2.88 | | 3.48 | Inflection Point | 60 mL |
| 1748 | D664-A | 1.87 | | -0.51 | Inflection Point | 125 mL |
| 1797 | | ---- | | ---- | --- | --- |
| 1850 | | ---- | | ---- | --- | --- |
| 1877 | | ---- | | ---- | --- | --- |
| 1969 | | ---- | | ---- | --- | --- |
| 2129 | D664-A | 1.94 | | -0.23 | --- | --- |
| 6016 | | ---- | | ---- | --- | --- |
| 6032 | | ---- | | ---- | --- | --- |
| 6183 | D664-A | 2.66 | | 2.61 | Inflection Point | 125 mL |
| 6197 | | ---- | | ---- | --- | --- |
| 6253 | | ---- | | ---- | --- | --- |
| 6284 | D974 | 1.88 | | -0.47 | --- | --- |
| 6310 | D664-A | 1.87 | | -0.51 | Buffer End Point (pH 10) | 60 mL |
| 6317 | | ---- | | ---- | --- | --- |
| 6320 | | ---- | | ---- | --- | --- |
| 6324 | | ---- | | ---- | --- | --- |

| | | | <u>Inflection Point only</u> | <u>BEP (pH 10 and 11) only</u> |
|----------------------|---------|-------------------|------------------------------|--------------------------------|
| normality | OK | | OK | OK |
| n | 37 | | 15 | 14 |
| outliers | 2 | | 1 | 0 |
| mean (n) | 1.9988 | | 2.3369 | 1.8509 |
| st.dev. (n) | 0.58759 | | 0.36838 | 0.45653 |
| R(calc.) | 1.6452 | | 1.0315 | 1.2783 |
| st.dev.(D664-A:18e2) | 0.25345 | | 0.25345 | --- |
| R(D664-A:18e2) | 0.7097 | IP 60mL | 0.8067 | --- |
| Compare: | | | | |
| R(D664-A:18e2) | 1.0893 | BEP (pH 10) 60 mL | --- | 1.0106 |
| R(D664-A:18e2) | 0.4506 | IP 125mL | 0.5304 | --- |
| R(D664-A:18e2) | 0.6545 | BEP (pH 10) 125mL | --- | 0.4159 |

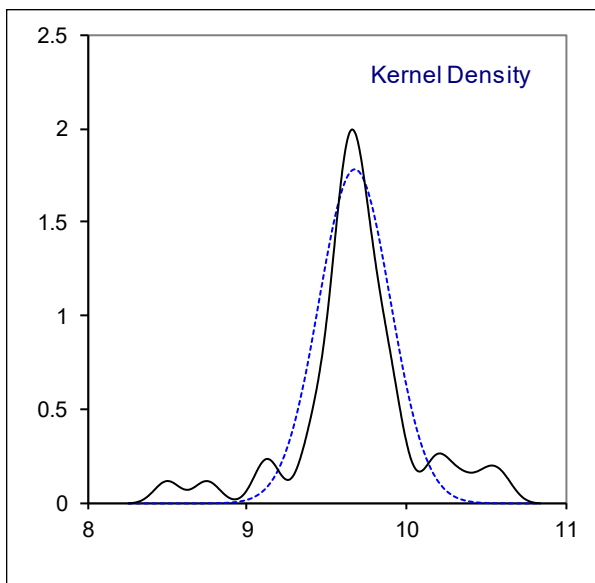
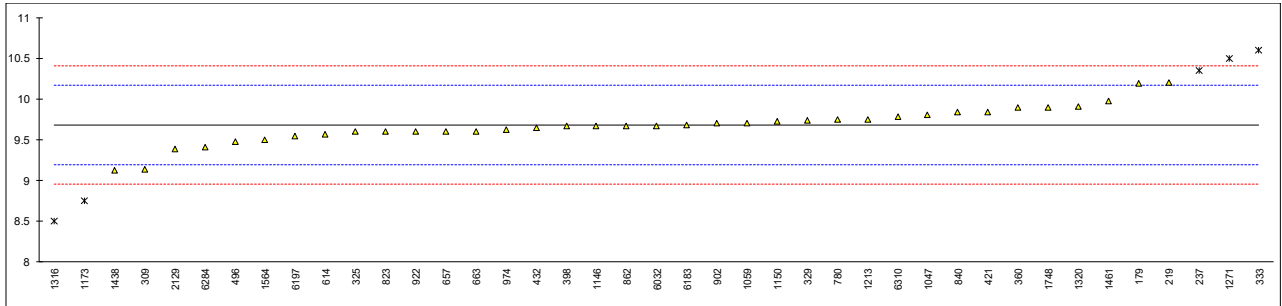
Lab 657 first reported 0.12



Determination of Base Number (HClO₄ titration) on sample #20075; results in mg KOH/g

| lab | method | value | mark | z(targ) | remarks |
|------|-----------------|--------|---------|---------|---------------------|
| 178 | | ---- | | ---- | |
| 179 | D2896-A forward | 10.19 | | 2.11 | |
| 211 | | ---- | | ---- | |
| 219 | D2896-A back | 10.2 | | 2.16 | |
| 237 | D2896-A back | 10.343 | R(0.05) | 2.75 | |
| 254 | | ---- | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | D2896-A back | 9.136 | | -2.24 | |
| 325 | D2896-B forward | 9.6 | | -0.32 | |
| 329 | D2896-A forward | 9.74 | | 0.25 | |
| 333 | D4739 | 10.6 | R(0.01) | 3.81 | |
| 339 | | ---- | | ---- | |
| 349 | | ---- | | ---- | |
| 360 | D2896-B forward | 9.89 | | 0.87 | |
| 398 | D2896-B forward | 9.665 | | -0.06 | |
| 421 | ISO3771 | 9.84 | | 0.67 | |
| 432 | D2896-B back | 9.64 | | -0.16 | |
| 496 | D2896-B back | 9.47 | | -0.86 | |
| 614 | D2896-B forward | 9.57 | | -0.45 | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D2896-B forward | 9.6 | | -0.32 | |
| 663 | D2896-B forward | 9.601 | | -0.32 | |
| 780 | D2896-B forward | 9.75 | | 0.30 | |
| 823 | D2896-A back | 9.6 | | -0.32 | |
| 840 | D2896-A forward | 9.84 | | 0.67 | |
| 862 | D2896-B forward | 9.67 | | -0.04 | |
| 875 | | ---- | | ---- | |
| 902 | D2896-B forward | 9.70 | | 0.09 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D2896-B forward | 9.6 | | -0.32 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D2896-A forward | 9.62 | | -0.24 | |
| 994 | | ---- | | ---- | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | ISO3771 | 9.8 | | 0.50 | |
| 1059 | ISO3771 | 9.7 | | 0.09 | |
| 1091 | | ---- | | ---- | |
| 1146 | D2896-A forward | 9.665 | | -0.06 | |
| 1150 | ISO3771 | 9.723 | | 0.18 | |
| 1173 | In house | 8.75 | R(0.01) | -3.84 | |
| 1213 | D2896-B forward | 9.75 | | 0.30 | |
| 1235 | | ---- | | ---- | |
| 1271 | ISO3771 | 10.50 | R(0.01) | 3.40 | |
| 1316 | D4739 | 8.5 | R(0.01) | -4.87 | |
| 1320 | D2896-B forward | 9.91 | | 0.96 | |
| 1409 | | ---- | | ---- | |
| 1412 | | ---- | | ---- | |
| 1438 | | 9.12 | | -2.31 | |
| 1461 | In house | 9.97 | | 1.20 | |
| 1510 | | ---- | | ---- | |
| 1564 | D2896-B back | 9.5 | C | -0.74 | first reported 11.2 |
| 1748 | D2896-A forward | 9.897 | | 0.90 | |
| 1797 | | ---- | | ---- | |
| 1850 | | ---- | | ---- | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | D2896-A back | 9.39 | | -1.19 | |
| 6016 | | ---- | | ---- | |
| 6032 | D2896-B forward | 9.67 | | -0.04 | |
| 6183 | D2896-A forward | 9.68 | | 0.01 | |
| 6197 | D2896-B forward | 9.54 | | -0.57 | |
| 6253 | | ---- | | ---- | |
| 6284 | D2896-A forward | 9.41 | | -1.11 | |
| 6310 | D2896-B forward | 9.78 | | 0.42 | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

| | |
|------------------------------|---------|
| normality | suspect |
| n | 36 |
| outliers | 5 |
| mean (n) | 9.679 |
| st.dev. (n) | 0.2244 |
| R(calc.) | 0.628 |
| st.dev. (D2896-A:15 forward) | 0.2420 |
| R(D2896-A:15 forward) | 0.677 |

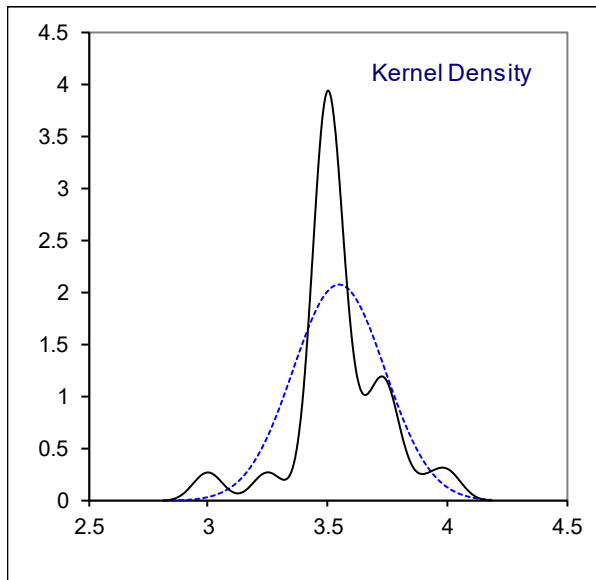
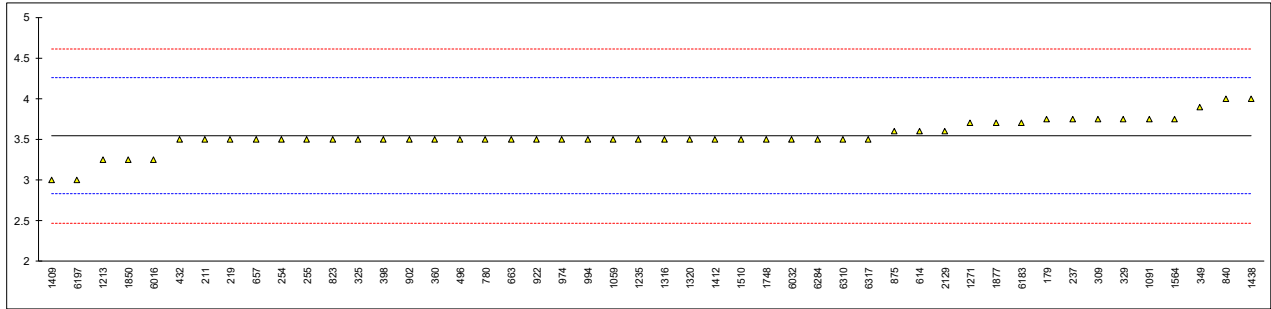


Determination of Color ASTM on sample #20075

| lab | method | reported test value | iis conversion * | mark | z(targ) |
|------|---------|---------------------|------------------|------|--------------------------|
| 178 | | ---- | ---- | | ---- |
| 179 | D1500 | L4.0 | 3.75 | | 0.58 |
| 211 | D1500 | 3.5 | 3.5 | | -0.12 |
| 219 | D1500 | 3.5 | 3.5 | | -0.12 |
| 237 | D1500 | L4.0 | 3.75 | | 0.58 |
| 254 | D1500 | 3.5 | 3.5 | | -0.12 |
| 255 | D1500 | 3.5 | 3.5 | | -0.12 |
| 257 | | ---- | ---- | | ---- |
| 309 | D1500 | L4.0 | 3.75 | | 0.58 |
| 325 | D6045 | 3.5 | 3.5 | | -0.12 |
| 329 | D1500 | L4.0 | 3.75 | | 0.58 |
| 333 | | ---- | ---- | | ---- |
| 339 | | ---- | ---- | | ---- |
| 349 | D6045 | 3.9 | 3.9 | C | 1.00 first reported 4.7 |
| 360 | D1500 | 3.5 | 3.5 | | -0.12 |
| 398 | D1500 | 3.5 | 3.5 | | -0.12 |
| 421 | | ---- | ---- | | ---- |
| 432 | D1500 | 3.5 | 3.5 | | -0.12 |
| 496 | D1500 | 3.5 | 3.5 | | -0.12 |
| 614 | D1500 | 3.6 | 3.6 | | 0.16 |
| 621 | | ---- | ---- | | ---- |
| 633 | | ---- | ---- | | ---- |
| 634 | | ---- | ---- | | ---- |
| 657 | D1500 | 3.5 | 3.5 | | -0.12 |
| 663 | D1500 | 3.5 | 3.5 | | -0.12 |
| 780 | D1500 | 3.5 | 3.5 | | -0.12 |
| 823 | D1500 | 3.5 | 3.5 | | -0.12 |
| 840 | D6045 | 4.0 | 4.0 | | 1.28 |
| 862 | | ---- | ---- | | ---- |
| 875 | D6045 | 3.6 | 3.6 | | 0.16 |
| 902 | D1500 | 3.5 | 3.5 | | -0.12 |
| 912 | | ---- | ---- | | ---- |
| 913 | | ---- | ---- | | ---- |
| 922 | D1500 | 3.5 | 3.5 | | -0.12 |
| 962 | | ---- | ---- | | ---- |
| 963 | | ---- | ---- | | ---- |
| 974 | D1500 | 3.5 | 3.5 | | -0.12 |
| 994 | D1500 | 3.5 | 3.5 | | -0.12 |
| 1011 | | ---- | ---- | | ---- |
| 1017 | | ---- | ---- | | ---- |
| 1047 | | ---- | ---- | | ---- |
| 1059 | D1500 | 3.5 | 3.5 | | -0.12 |
| 1091 | D1500 | L4.0 | 3.75 | | 0.58 |
| 1146 | | ---- | ---- | | ---- |
| 1150 | | ---- | ---- | | ---- |
| 1173 | | ---- | ---- | | ---- |
| 1213 | D1500 | L 3.5 | 3.25 | | -0.82 |
| 1235 | ISO2049 | 3.5 | 3.5 | | -0.12 |
| 1271 | D6045 | 3.7 | 3.7 | | 0.44 |
| 1316 | D1500 | 3.5 | 3.5 | | -0.12 |
| 1320 | D1500 | 3.5 | 3.5 | | -0.12 |
| 1409 | D1500 | 3.0 | 3.0 | | -1.52 |
| 1412 | D1500 | 3.5 | 3.5 | | -0.12 |
| 1438 | | 4.0 | 4.0 | | 1.28 |
| 1461 | | ---- | ---- | | ---- |
| 1510 | D1500 | 3.5 | 3.5 | | -0.12 |
| 1564 | D1500 | L4 | 3.75 | | 0.58 |
| 1748 | D1500 | 3.5 | 3.5 | | -0.12 |
| 1797 | | ---- | ---- | | ---- |
| 1850 | D1500 | L3,5 | 3.25 | | -0.82 |
| 1877 | D6045 | 3.7 | 3.7 | | 0.44 |
| 1969 | | ---- | ---- | | ---- |
| 2129 | D6045 | 3.6 | 3.6 | | 0.16 |
| 6016 | D1500 | <3.5 | 3.25 | | -0.82 |
| 6032 | D1500 | 3.5 | 3.5 | | -0.12 |
| 6183 | D1500 | 3.7 | 3.7 | | 0.44 |
| 6197 | D1500 | 3.0 | 3.0 | C | -1.52 first reported 2.0 |
| 6253 | | ---- | ---- | | ---- |
| 6284 | D1500 | 3.5 | 3.5 | | -0.12 |
| 6310 | D1500 | 3.5 | 3.5 | | -0.12 |
| 6317 | D1500 | 3.5 | 3.5 | | -0.12 |
| 6320 | | ---- | ---- | | ---- |
| 6324 | | ---- | ---- | | ---- |

| | |
|-------------------|--------|
| normality | not OK |
| n | 48 |
| outliers | 0 |
| mean (n) | 3.54 |
| st.dev. (n) | 0.195 |
| R(calc.) | 0.55 |
| st.dev.(D1500:12) | 0.357 |
| R(D1500:12) | 1 |

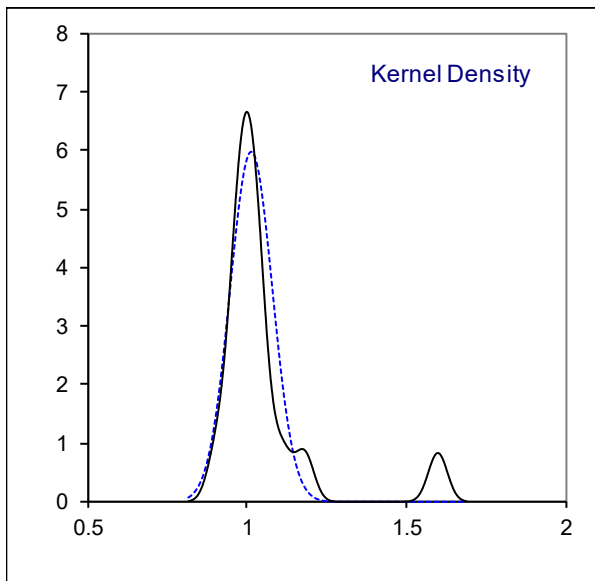
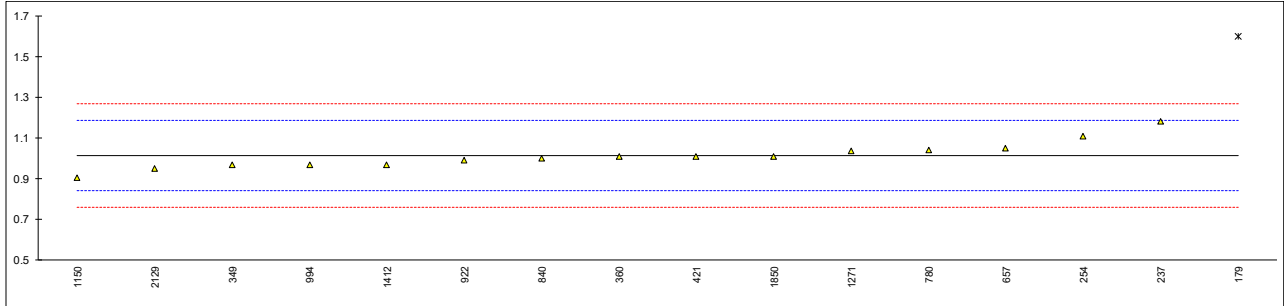
*) In the calculation of the mean, standard deviation and the reproducibility in this column, a reported value of 'L y' is changed tot y-0.25 (for example L3.5 into 3.25).



Determination of Conradson Carbon Residue on sample #20075; results in %M/M

| lab | method | value | mark | z(targ) | remarks |
|------|---------|--------|---------|---------|---------|
| 178 | | ---- | | ---- | |
| 179 | D189 | 1.60 | G(0.01) | 6.89 | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | D189 | 1.18 | | 1.96 | |
| 254 | D189 | 1.11 | | 1.14 | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | ---- | | ---- | |
| 325 | | ---- | | ---- | |
| 329 | | ---- | | ---- | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | D189 | 0.97 | | -0.51 | |
| 360 | ISO6615 | 1.009 | | -0.05 | |
| 398 | | ---- | | ---- | |
| 421 | ISO6615 | 1.01 | | -0.04 | |
| 432 | | ---- | | ---- | |
| 496 | | ---- | | ---- | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D189 | 1.05 | | 0.43 | |
| 663 | | ---- | | ---- | |
| 780 | D189 | 1.04 | | 0.32 | |
| 823 | | ---- | | ---- | |
| 840 | D189 | 1.000 | | -0.15 | |
| 862 | | ---- | | ---- | |
| 875 | | ---- | | ---- | |
| 902 | | ---- | | ---- | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D189 | 0.99 | | -0.27 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | | ---- | | ---- | |
| 994 | D189 | 0.97 | | -0.51 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | ---- | | ---- | |
| 1059 | | ---- | | ---- | |
| 1091 | | ---- | | ---- | |
| 1146 | | ---- | | ---- | |
| 1150 | ISO6615 | 0.9049 | | -1.27 | |
| 1173 | | ---- | | ---- | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | ISO6615 | 1.035 | | 0.26 | |
| 1316 | | ---- | | ---- | |
| 1320 | | ---- | | ---- | |
| 1409 | | ---- | | ---- | |
| 1412 | D189 | 0.97 | | -0.51 | |
| 1438 | | ---- | | ---- | |
| 1461 | | ---- | | ---- | |
| 1510 | | ---- | | ---- | |
| 1564 | | ---- | | ---- | |
| 1748 | | ---- | | ---- | |
| 1797 | | ---- | | ---- | |
| 1850 | ISO6615 | 1.01 | | -0.04 | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | D189 | 0.948 | | -0.76 | |
| 6016 | | ---- | | ---- | |
| 6032 | | ---- | | ---- | |
| 6183 | | ---- | | ---- | |
| 6197 | | ---- | | ---- | |
| 6253 | | ---- | | ---- | |
| 6284 | | ---- | | ---- | |
| 6310 | | ---- | | ---- | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

| | |
|------------------|--------|
| normality | not OK |
| n | 15 |
| outliers | 1 |
| mean (n) | 1.013 |
| st.dev. (n) | 0.0666 |
| R(calc.) | 0.186 |
| st.dev.(D189:06) | 0.0852 |
| R(D189:06) | 0.238 |



Determination of Ramsbottom Carbon Residue on sample #20075; results in %M/M

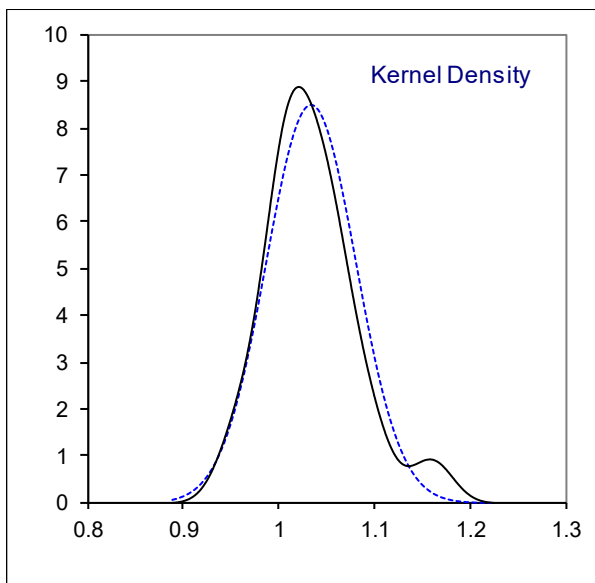
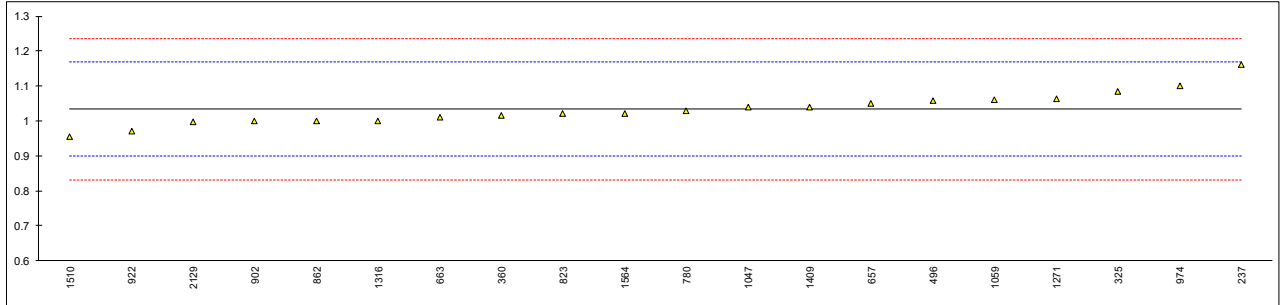
| lab | method | value | mark | z(targ) | remarks |
|------|----------|-------|------|---------|---------|
| 178 | | ---- | | ---- | |
| 179 | D524 | 0.83 | | ---- | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | | ---- | | ---- | |
| 254 | | ---- | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | ---- | | ---- | |
| 325 | | ---- | | ---- | |
| 329 | | ---- | | ---- | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | | ---- | | ---- | |
| 360 | | ---- | | ---- | |
| 398 | | ---- | | ---- | |
| 421 | | ---- | | ---- | |
| 432 | | ---- | | ---- | |
| 496 | | ---- | | ---- | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D524 | 0.75 | | ---- | |
| 663 | | ---- | | ---- | |
| 780 | | ---- | | ---- | |
| 823 | | ---- | | ---- | |
| 840 | | ---- | | ---- | |
| 862 | | ---- | | ---- | |
| 875 | | ---- | | ---- | |
| 902 | | ---- | | ---- | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | | ---- | | ---- | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | | ---- | | ---- | |
| 994 | | ---- | | ---- | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | ---- | | ---- | |
| 1059 | | ---- | | ---- | |
| 1091 | | ---- | | ---- | |
| 1146 | | ---- | | ---- | |
| 1150 | | ---- | | ---- | |
| 1173 | | ---- | | ---- | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | | ---- | | ---- | |
| 1316 | | ---- | | ---- | |
| 1320 | | ---- | | ---- | |
| 1409 | | ---- | | ---- | |
| 1412 | | ---- | | ---- | |
| 1438 | | ---- | | ---- | |
| 1461 | | ---- | | ---- | |
| 1510 | | ---- | | ---- | |
| 1564 | | ---- | | ---- | |
| 1748 | | ---- | | ---- | |
| 1797 | | ---- | | ---- | |
| 1850 | | ---- | | ---- | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | | ---- | | ---- | |
| 6016 | | ---- | | ---- | |
| 6032 | | ---- | | ---- | |
| 6183 | | ---- | | ---- | |
| 6197 | | ---- | | ---- | |
| 6253 | | ---- | | ---- | |
| 6284 | | ---- | | ---- | |
| 6310 | | ---- | | ---- | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |
| | n | 2 | | | |
| | mean (n) | <1 | | | |

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Determination of Carbon Residue (micro method) on sample #20075; results in %M/M

| lab | method | value | mark | z(targ) | remarks |
|------|----------|--------|------|---------|---------|
| 178 | | ---- | | ---- | |
| 179 | | ---- | | ---- | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | D4530 | 1.16 | | 1.87 | |
| 254 | | ---- | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | ---- | | ---- | |
| 325 | D4530 | 1.0839 | | 0.74 | |
| 329 | | ---- | | ---- | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | | ---- | | ---- | |
| 360 | ISO10370 | 1.017 | | -0.25 | |
| 398 | | ---- | | ---- | |
| 421 | | ---- | | ---- | |
| 432 | | ---- | | ---- | |
| 496 | D4530 | 1.057 | | 0.35 | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D4530 | 1.05 | | 0.24 | |
| 663 | D4530 | 1.0116 | | -0.33 | |
| 780 | D4530 | 1.03 | | -0.06 | |
| 823 | ISO10370 | 1.02 | | -0.20 | |
| 840 | | ---- | | ---- | |
| 862 | D4530 | 1.00 | | -0.50 | |
| 875 | | ---- | | ---- | |
| 902 | D4530 | 1.00 | | -0.50 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D4530 | 0.97 | | -0.94 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D4530 | 1.10 | | 0.98 | |
| 994 | | ---- | | ---- | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | ISO10370 | 1.04 | | 0.09 | |
| 1059 | ISO10370 | 1.06 | | 0.39 | |
| 1091 | | ---- | | ---- | |
| 1146 | | ---- | | ---- | |
| 1150 | | ---- | | ---- | |
| 1173 | | ---- | | ---- | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | ISO10370 | 1.064 | | 0.45 | |
| 1316 | D4530 | 1.00 | | -0.50 | |
| 1320 | | ---- | | ---- | |
| 1409 | D4530 | 1.04 | | 0.09 | |
| 1412 | | ---- | | ---- | |
| 1438 | | ---- | | ---- | |
| 1461 | | ---- | | ---- | |
| 1510 | D4530 | 0.954 | | -1.18 | |
| 1564 | D4530 | 1.02 | | -0.20 | |
| 1748 | | ---- | | ---- | |
| 1797 | | ---- | | ---- | |
| 1850 | | ---- | | ---- | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | ISO10370 | 0.997 | | -0.54 | |
| 6016 | | ---- | | ---- | |
| 6032 | | ---- | | ---- | |
| 6183 | | ---- | | ---- | |
| 6197 | | ---- | | ---- | |
| 6253 | | ---- | | ---- | |
| 6284 | | ---- | | ---- | |
| 6310 | | ---- | | ---- | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

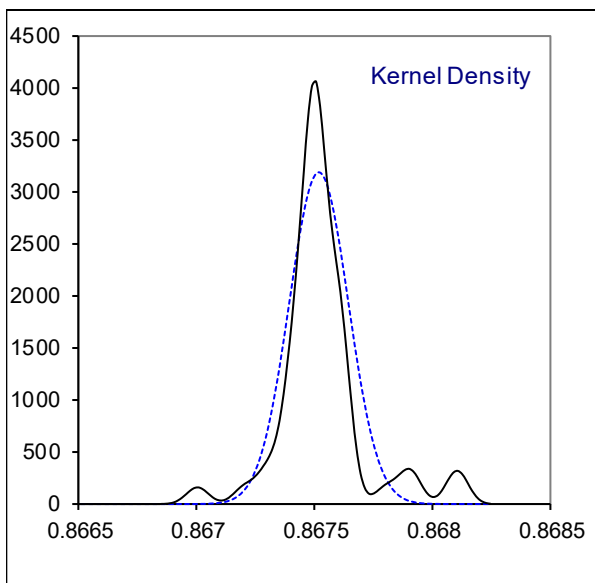
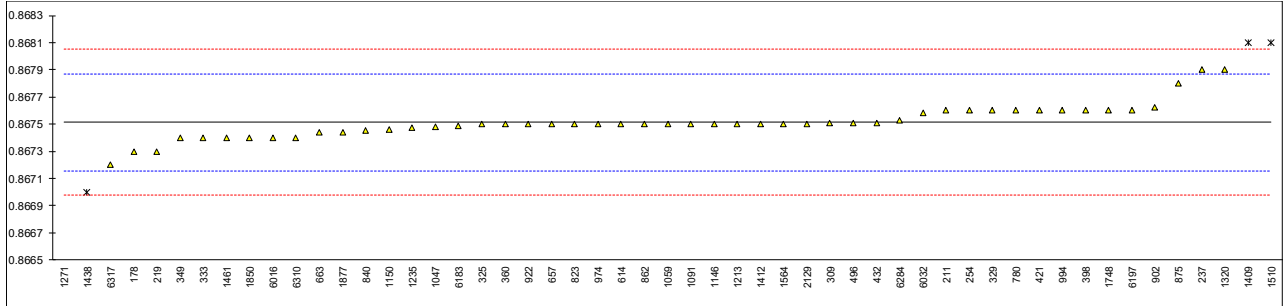
| | |
|--------------------|---------|
| normality | suspect |
| n | 20 |
| outliers | 0 |
| mean (n) | 1.034 |
| st.dev. (n) | 0.0468 |
| R(calc.) | 0.131 |
| st.dev. (D4530:15) | 0.0674 |
| R(D4530:15) | 0.189 |



Determination of Density at 15°C on sample #20075; results in kg/L

| lab | method | value | mark | z(targ) | remarks |
|------|----------|----------|-----------|---------|--|
| 178 | D4052 | 0.8673 | | -1.20 | |
| 179 | | ---- | | ---- | |
| 211 | D4052 | 0.8676 | | 0.48 | |
| 219 | D1298 | 0.8673 | | -1.20 | |
| 237 | D4052 | 0.8679 | | 2.16 | |
| 254 | D4052 | 0.8676 | | 0.48 | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | D4052 | 0.86751 | | -0.02 | |
| 325 | D4052 | 0.8675 | | -0.08 | |
| 329 | D4052 | 0.8676 | | 0.48 | |
| 333 | D4052 | 0.8674 | | -0.64 | |
| 339 | | ---- | | ---- | |
| 349 | D4052 | 0.8674 | | -0.64 | |
| 360 | ISO12185 | 0.8675 | | -0.08 | |
| 398 | ISO12185 | 0.8676 | | 0.48 | |
| 421 | ISO12185 | 0.8676 | | 0.48 | |
| 432 | ISO12185 | 0.86751 | | -0.02 | |
| 496 | ISO12185 | 0.86751 | | -0.02 | |
| 614 | D4052 | 0.8675 | | -0.08 | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D4052 | 0.8675 | | -0.08 | |
| 663 | D4052 | 0.86744 | | -0.42 | |
| 780 | ISO12185 | 0.8676 | C | 0.48 | first reported 868.1 kg/m ³ |
| 823 | D4052 | 0.8675 | | -0.08 | |
| 840 | D4052 | 0.86745 | | -0.36 | |
| 862 | D4052 | 0.8675 | | -0.08 | |
| 875 | D4052 | 0.8678 | | 1.60 | |
| 902 | D4052 | 0.86762 | | 0.59 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D4052 | 0.8675 | | -0.08 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D4052 | 0.8675 | | -0.08 | |
| 994 | ISO12185 | 0.8676 | | 0.48 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | ISO12185 | 0.86748 | | -0.19 | |
| 1059 | ISO12185 | 0.8675 | | -0.08 | |
| 1091 | D4052 | 0.8675 | | -0.08 | |
| 1146 | D4052 | 0.8675 | | -0.08 | |
| 1150 | ISO12185 | 0.86746 | | -0.30 | |
| 1173 | | ---- | | ---- | |
| 1213 | D4052 | 0.86750 | | -0.08 | |
| 1235 | ISO12185 | 0.867475 | | -0.22 | |
| 1271 | D4052 | 0.8640 | C,R(0.01) | -19.68 | first reported 868.1 kg/m ³ |
| 1316 | | ---- | | ---- | |
| 1320 | ISO12185 | 0.8679 | | 2.16 | |
| 1409 | ISO12185 | 0.8681 | C,R(0.01) | 3.28 | first reported 868.1 without unit |
| 1412 | D4052 | 0.8675 | | -0.08 | |
| 1438 | D1298 | 0.867 | C,R(0.01) | -2.88 | first reported 0.865 |
| 1461 | ISO3675 | 0.8674 | | -0.64 | |
| 1510 | ISO12185 | 0.8681 | R(0.01) | 3.28 | |
| 1564 | D4052 | 0.8675 | | -0.08 | |
| 1748 | D4052 | 0.8676 | | 0.48 | |
| 1797 | | ---- | | ---- | |
| 1850 | D4052 | 0.8674 | | -0.64 | |
| 1877 | D4052 | 0.86744 | | -0.42 | |
| 1969 | | ---- | | ---- | |
| 2129 | D4052 | 0.8675 | | -0.08 | |
| 6016 | D4052 | 0.8674 | | -0.64 | |
| 6032 | D4052 | 0.86758 | | 0.37 | |
| 6183 | D4052 | 0.867488 | | -0.15 | |
| 6197 | D4052 | 0.8676 | | 0.48 | |
| 6253 | | ---- | | ---- | |
| 6284 | D4052 | 0.86753 | | 0.09 | |
| 6310 | D4052 | 0.8674 | | -0.64 | |
| 6317 | D7042 | 0.8672 | | -1.76 | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

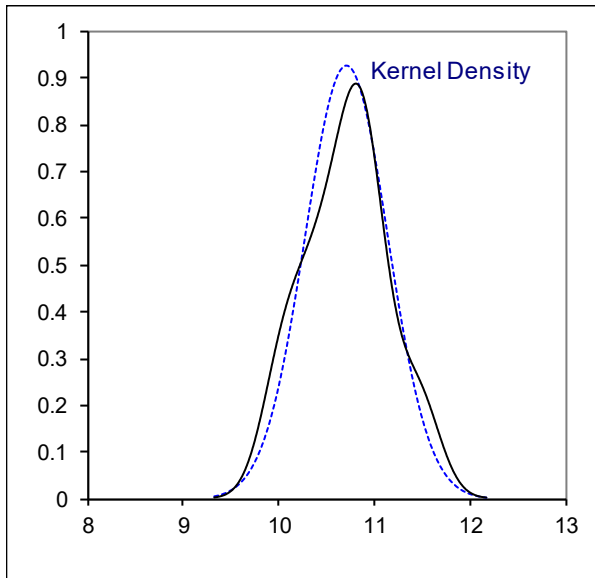
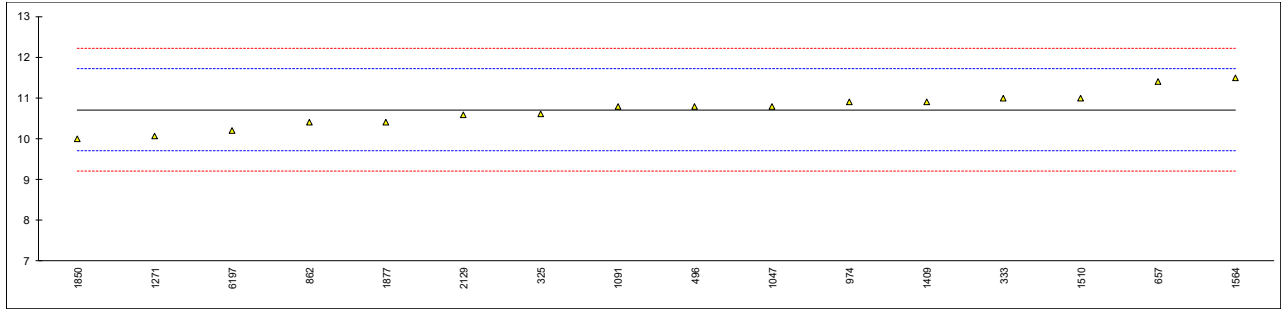
| | |
|----------------------|----------|
| normality | not OK |
| n | 49 |
| outliers | 4 |
| mean (n) | 0.86751 |
| st.dev. (n) | 0.000125 |
| R(calc.) | 0.00035 |
| st.dev.(ISO12185:96) | 0.0002 |
| R(ISO12185:96) | 0.0005 |



Determination of Evaporation loss by Noack on sample #20075; results in %M/M

| lab | method | value | mark | z(targ) | remarks |
|------|-------------|-------|------|---------|---------|
| 178 | | ---- | | ---- | |
| 179 | | ---- | | ---- | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | | ---- | | ---- | |
| 254 | | ---- | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | ---- | | ---- | |
| 325 | CEC L-40-93 | 10.6 | | -0.22 | |
| 329 | | ---- | | ---- | |
| 333 | CEC L-40-93 | 11.0 | | 0.58 | |
| 339 | | ---- | | ---- | |
| 349 | | ---- | | ---- | |
| 360 | | ---- | | ---- | |
| 398 | | ---- | | ---- | |
| 421 | | ---- | | ---- | |
| 432 | | ---- | | ---- | |
| 496 | D5800-B | 10.8 | | 0.18 | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D5800-B | 11.4 | | 1.37 | |
| 663 | | ---- | | ---- | |
| 780 | | ---- | | ---- | |
| 823 | | ---- | | ---- | |
| 840 | | ---- | | ---- | |
| 862 | D5800-B | 10.4 | | -0.62 | |
| 875 | | ---- | | ---- | |
| 902 | | ---- | | ---- | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | | ---- | | ---- | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D5800-B | 10.9 | | 0.38 | |
| 994 | | ---- | | ---- | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | DIN51581 | 10.8 | | 0.18 | |
| 1059 | | ---- | | ---- | |
| 1091 | D5800-B | 10.8 | | 0.18 | |
| 1146 | | ---- | | ---- | |
| 1150 | | ---- | | ---- | |
| 1173 | | ---- | | ---- | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | DIN51581 | 10.06 | | -1.29 | |
| 1316 | | ---- | | ---- | |
| 1320 | | ---- | | ---- | |
| 1409 | D5800-B | 10.9 | | 0.38 | |
| 1412 | | ---- | | ---- | |
| 1438 | | ---- | | ---- | |
| 1461 | | ---- | | ---- | |
| 1510 | D5800-B | 11.0 | | 0.58 | |
| 1564 | DIN51581 | 11.5 | | 1.57 | |
| 1748 | | ---- | | ---- | |
| 1797 | | ---- | | ---- | |
| 1850 | DIN51581 | 10.0 | | -1.41 | |
| 1877 | CEC L-40-93 | 10.4 | | -0.62 | |
| 1969 | | ---- | | ---- | |
| 2129 | D5800-A | 10.59 | | -0.24 | |
| 6016 | | ---- | | ---- | |
| 6032 | | ---- | | ---- | |
| 6183 | | ---- | | ---- | |
| 6197 | D5800-B | 10.2 | | -1.01 | |
| 6253 | | ---- | | ---- | |
| 6284 | | ---- | | ---- | |
| 6310 | | ---- | | ---- | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

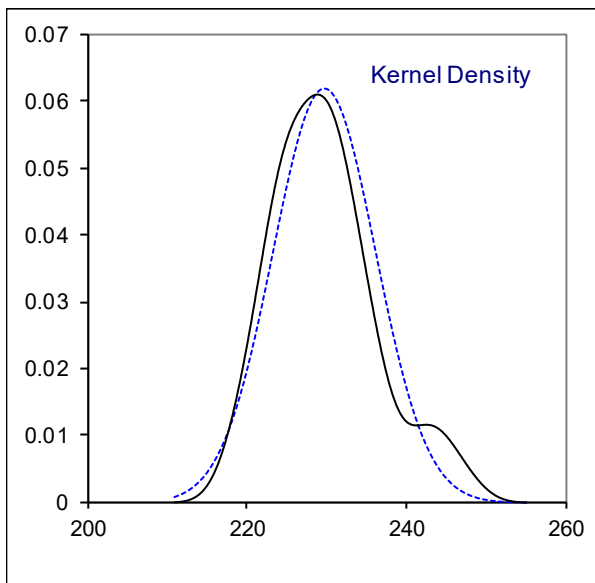
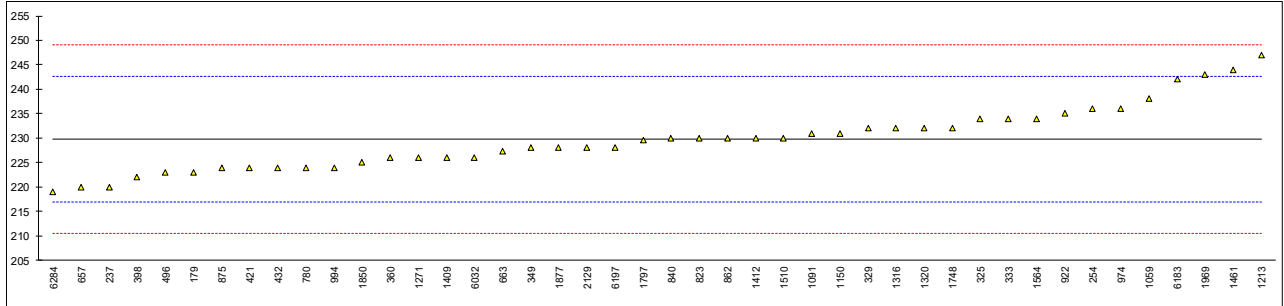
| | | | |
|----------------------|--------|------------------------|----------------------|
| | | <u>D5800-A/DIN1581</u> | <u>D5800-B only:</u> |
| normality | OK | OK | OK |
| n | 16 | 5 | 8 |
| outliers | 0 | 0 | 0 |
| mean (n) | 10.709 | 10.590 | 10.800 |
| st.dev. (n) | 0.4298 | 0.6126 | 0.3665 |
| R(calc.) | 1.203 | 1.715 | 1.026 |
| st.dev.(D5800-B:19a) | 0.5029 | --- | 0.5029 |
| R(D5800-B:19a) | 1.408 | --- | 1.417 |
| Compare | | | |
| R(D5800-A:19a) | 1.960 | 1.938 | --- |



Determination of Flash Point C.O.C. on sample #20075; results in °C

| lab | method | value | mark | z(targ) | remarks |
|------|---------|---------|------|---------|---------|
| 178 | | ---- | | ---- | |
| 179 | D92 | 223 | | -1.05 | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | D92 | 220 | | -1.51 | |
| 254 | D92 | 236 | | 0.98 | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | ---- | | ---- | |
| 325 | D92 | 234 | | 0.67 | |
| 329 | D92 | 232 | | 0.35 | |
| 333 | D92 | 234 | | 0.67 | |
| 339 | | ---- | | ---- | |
| 349 | D92 | 228 | | -0.27 | |
| 360 | ISO2592 | 226 | | -0.58 | |
| 398 | D92 | 222 | | -1.20 | |
| 421 | ISO2592 | 224 | | -0.89 | |
| 432 | D92 | 224 | | -0.89 | |
| 496 | D92 | 223 | | -1.05 | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D92 | 220 | | -1.51 | |
| 663 | D92 | 227.375 | | -0.37 | |
| 780 | D92 | 224.0 | | -0.89 | |
| 823 | D92 | 230 | | 0.04 | |
| 840 | D92 | 230 | | 0.04 | |
| 862 | D92 | 230 | | 0.04 | |
| 875 | D92 | 224 | | -0.89 | |
| 902 | | ---- | | ---- | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D92 | 235 | | 0.82 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D92 | 236 | | 0.98 | |
| 994 | D92 | 224.0 | | -0.89 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | ---- | | ---- | |
| 1059 | ISO2592 | 238 | | 1.29 | |
| 1091 | D92 | 231.0 | | 0.20 | |
| 1146 | | ---- | | ---- | |
| 1150 | ISO2592 | 231 | | 0.20 | |
| 1173 | | ---- | | ---- | |
| 1213 | D92 | 247 | | 2.69 | |
| 1235 | | ---- | | ---- | |
| 1271 | ISO2592 | 226 | | -0.58 | |
| 1316 | D92 | 232 | | 0.35 | |
| 1320 | D92 | 232 | | 0.35 | |
| 1409 | ISO2592 | 226 | | -0.58 | |
| 1412 | D92 | 230.0 | | 0.04 | |
| 1438 | | ---- | | ---- | |
| 1461 | ISO2592 | 244 | | 2.22 | |
| 1510 | D92 | 230 | | 0.04 | |
| 1564 | D92 | 234 | | 0.67 | |
| 1748 | D92 | 232 | | 0.35 | |
| 1797 | ISO2592 | 229.5 | | -0.03 | |
| 1850 | ISO2592 | 225 | | -0.73 | |
| 1877 | D92 | 228 | | -0.27 | |
| 1969 | ISO2592 | 242.925 | | 2.05 | |
| 2129 | D92 | 228.0 | | -0.27 | |
| 6016 | | ---- | | ---- | |
| 6032 | D92 | 226 | | -0.58 | |
| 6183 | D92 | 242.0 | | 1.91 | |
| 6197 | D92 | 228 | | -0.27 | |
| 6253 | | ---- | | ---- | |
| 6284 | D92 | 219 | | -1.67 | |
| 6310 | | ---- | | ---- | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

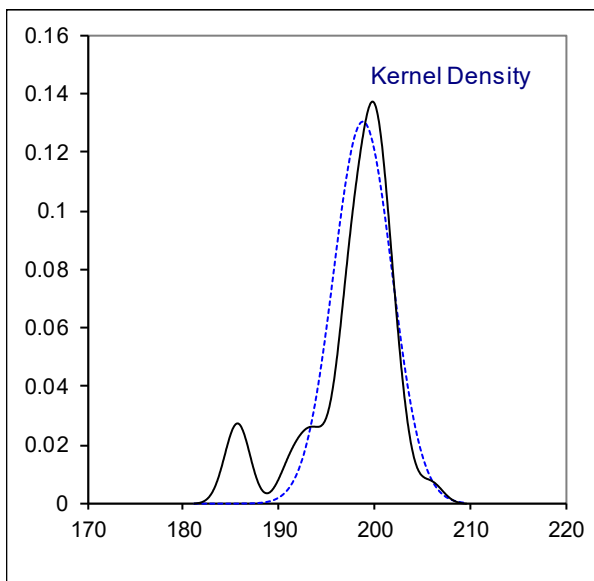
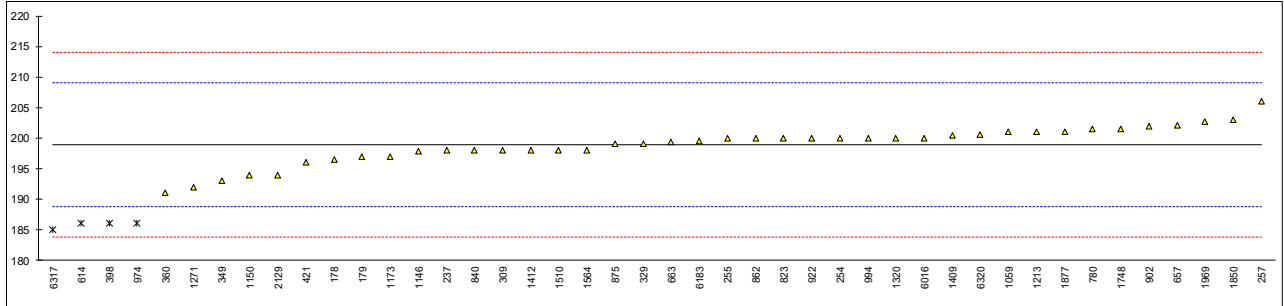
| | |
|-----------------|--------|
| normality | OK |
| n | 44 |
| outliers | 0 |
| mean (n) | 229.72 |
| st.dev. (n) | 6.461 |
| R(calc.) | 18.09 |
| st.dev.(D92:18) | 6.429 |
| R(D92:18) | 18 |



Determination of Flash Point PMcc on sample #20075; results in °C

| lab | method | value | mark | z(targ) | remarks |
|------|-----------|---------|---------|---------|--------------------|
| 178 | D93-A | 196.5 | | -0.48 | |
| 179 | D93-A | 197.0 | | -0.38 | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | D93-B | 198.0 | | -0.18 | |
| 254 | D93-A | 200 | | 0.22 | |
| 255 | D93-A | 200.0 | | 0.22 | |
| 257 | D93-A | 206.0 | | 1.41 | |
| 309 | D93-A | 198.0 | | -0.18 | |
| 325 | | ---- | | ---- | |
| 329 | D93-A | 199 | | 0.02 | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | D93-A | 193 | | -1.17 | |
| 360 | ISO2719-A | 191.0 | | -1.57 | |
| 398 | D93-A | 186 | R(0.01) | -2.56 | |
| 421 | D93-A | 196.0 | | -0.58 | |
| 432 | | ---- | | ---- | |
| 496 | | ---- | | ---- | |
| 614 | D93-A | 186 | R(0.01) | -2.56 | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D93-A | 202.1 | | 0.63 | |
| 663 | D93-A | 199.375 | | 0.09 | |
| 780 | D93-A | 201.5 | | 0.52 | |
| 823 | D93-B | 200 | | 0.22 | |
| 840 | D93-A | 198 | | -0.18 | |
| 862 | D93-A | 200 | | 0.22 | |
| 875 | D93-A | 199.0 | | 0.02 | |
| 902 | D93-A | 202 | | 0.61 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D93-A | 200 | | 0.22 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D93-A | 186 | R(0.01) | -2.56 | |
| 994 | D93-A | 200.0 | | 0.22 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | ---- | | ---- | |
| 1059 | ISO2719-A | 201.0 | | 0.42 | |
| 1091 | | ---- | | ---- | |
| 1146 | D93-A | 197.8 | | -0.22 | |
| 1150 | ISO2719-A | 194.0 | | -0.97 | |
| 1173 | D93-A | 197.0 | | -0.38 | |
| 1213 | D93-A | 201 | | 0.42 | |
| 1235 | | ---- | | ---- | |
| 1271 | ISO2719-A | 192 | C | -1.37 | first reported 216 |
| 1316 | | ---- | | ---- | |
| 1320 | ISO2719-A | 200 | | 0.22 | |
| 1409 | D93-A | 200.5 | | 0.32 | |
| 1412 | D93-A | 198.0 | | -0.18 | |
| 1438 | | ---- | | ---- | |
| 1461 | | ---- | | ---- | |
| 1510 | D93-A | 198 | | -0.18 | |
| 1564 | D93-A | 198 | | -0.18 | |
| 1748 | D93-A | 201.5 | | 0.52 | |
| 1797 | | ---- | | ---- | |
| 1850 | ISO2719-A | 203 | | 0.81 | |
| 1877 | D93-A | 201.0 | | 0.42 | |
| 1969 | ISO2719-A | 202.71 | | 0.75 | |
| 2129 | D93-A | 194.0 | | -0.97 | |
| 6016 | D93-A | 200 | | 0.22 | |
| 6032 | | ---- | | ---- | |
| 6183 | D93-A | 199.5 | | 0.12 | |
| 6197 | | ---- | | ---- | |
| 6253 | | ---- | | ---- | |
| 6284 | | ---- | | ---- | |
| 6310 | | ---- | | ---- | |
| 6317 | D93-B | 185 | R(0.01) | -2.76 | |
| 6320 | ISO2719-A | 200.6 | | 0.34 | |
| 6324 | | ---- | | ---- | |

| | |
|-------------------|--------|
| normality | OK |
| n | 40 |
| outliers | 4 |
| mean (n) | 198.90 |
| st.dev. (n) | 3.057 |
| R(calc.) | 8.56 |
| st.dev.(D93-A:19) | 5.044 |
| R(D93-A:19) | 14.12 |



Determination of Foaming Tendency, 5 min blowing period on sample #20075; results in mL

| lab | method | sample used | diffuser | Seq. I | mark | z(targ) | Seq. II | mark | z(targ) | Seq. III | mark | z(targ) |
|------|---------|-------------------|----------|--------|------|---------|---------|------|---------|----------|------|---------|
| 178 | | | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 179 | D892 | As received | Metal | 20 | | 2.05 | 30 | | 0.08 | 10 | | 1.07 |
| 211 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 219 | D892 | As received | Stone | 0 | | -1.21 | 20 | C | -0.97 | 0 | | -0.72 |
| 237 | D892 | After agitation A | Metal | 10 | | 0.42 | 30 | | 0.08 | 10 | | 1.07 |
| 254 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 255 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 257 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 309 | D892 | After agitation A | Metal | 20 | | 2.05 | 40 | | 1.12 | 10 | | 1.07 |
| 325 | D892 | As received | Metal | 0 | | -1.21 | 50 | | 2.17 | 0 | | -0.72 |
| 329 | D892 | As received | Stone | 0 | | -1.21 | 20 | | -0.97 | 0 | | -0.72 |
| 333 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 339 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 349 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 360 | ISO6247 | As received | Stone | 5 | | -0.39 | 10 | | -2.01 | 0 | | -0.72 |
| 398 | D892 | As received | Stone | 5 | | -0.39 | 20 | | -0.97 | 5 | | 0.18 |
| 421 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 432 | D892 | As received | Stone | 0 | | -1.21 | 30 | | 0.08 | 0 | | -0.72 |
| 496 | D892 | As received | Metal | 0 | | -1.21 | 40 | | 1.12 | 0 | | -0.72 |
| 614 | D892 | As received | Metal | 10 | | 0.42 | 10 | | -2.01 | 10 | | 1.07 |
| 621 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 633 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 634 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 657 | D892 | As received | Stone | NIL | | ---- | 60 | | 3.21 | NIL | | ---- |
| 663 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 780 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 823 | D892 | As received | Stone | 10 | | 0.42 | 20 | | -0.97 | 10 | | 1.07 |
| 840 | D892 | As received | Stone | 0 | | -1.21 | 10 | | -2.01 | 0 | | -0.72 |
| 862 | D892 | As received | Metal | 0 | | -1.21 | 20 | | -0.97 | 0 | | -0.72 |
| 875 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 902 | D892 | After agitation A | Metal | 20 | | 2.05 | 80 | R1 | 5.31 | 20 | R1 | 2.86 |
| 912 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 913 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 922 | D892 | As received | Stone | 0 | | -1.21 | 20 | C | -0.97 | 0 | | -0.72 |
| 962 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 963 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 974 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 994 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1011 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1017 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1047 | D892 | --- | --- | 0 | | -1.21 | 55 | | 2.69 | 0 | | -0.72 |
| 1059 | D892 | As received | Metal | 20 | | 2.05 | 60 | | 3.21 | nil | | ---- |
| 1091 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1146 | D892 | As received | Metal | 20 | | 2.05 | 30 | | 0.08 | 10 | | 1.07 |
| 1150 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1173 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1213 | | --- | --- | ---- | | ---- | 5 | | -2.54 | ---- | | ---- |
| 1235 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1271 | ISO6247 | As received | Stone | 5 | | -0.39 | 20 | | -0.97 | 5 | | 0.18 |
| 1316 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1320 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1409 | D892 | After agitation A | Metal | 20 | | 2.05 | 50 | | 2.17 | 0 | | -0.72 |
| 1412 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1438 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1461 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1510 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1564 | D892 | As received | Stone | 10 | | 0.42 | 40 | | 1.12 | 10 | | 1.07 |
| 1748 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1797 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1850 | ISO6247 | As received | Stone | 5 | | -0.39 | 120 | R1 | 9.49 | 0 | | -0.72 |
| 1877 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1969 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 2129 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6016 | | **) | Stone | 10 | | 0.42 | 15 | C | -1.49 | 10 | | 1.07 |
| 6032 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6183 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6197 | | After agitation A | Metal | 10 | | 0.42 | 20 | | -0.97 | 10 | | 1.07 |
| 6253 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6284 | D892 | **) | Stone | 0 | | -1.21 | 25 | | -0.45 | 0 | | -0.72 |
| 6310 | D892 | After agitation A | Metal | 0 | | -1.21 | 40 | | 1.12 | 0 | | -0.72 |
| 6317 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6320 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6324 | | --- | --- | ---- | | ---- | ---- | | ---- | ---- | | ---- |

| lab | method | sample used | diffuser | Seq. I | mark | z(targ) | Seq. II | mark | z(targ) | Seq. III | mark | z(targ) |
|-----|---------------------|-------------|----------|--------|------|---------|---------|------|---------|----------|------|---------|
| | normality | | | OK | | | OK | | | OK | | |
| | n | | | 27 | | | 27 | | | 25 | | |
| | outliers | | | 0 | | | 2 | | | 1 | | |
| | mean (n) | | | 7.41 | | | 29.26 | | | 4.00 | | |
| | st.dev. (n) | | | 7.890 | | | 15.793 | | | 4.787 | | |
| | R(calc.) | | | 22.09 | | | 44.22 | | | 13.40 | | |
| | st.dev.(D892:13e1)* | | | 6.128 | | | 9.562 | | | 5.593 | | |
| | R(D892:13e1)* | | | 17.16 | | | 26.77 | | | 15.66 | | |
| | Compare | | | | | | | | | | | |
| | R(D892:18)* | | | 5.46 | | | 24.88 | | | 7.00 | | |

Lab 219 first reported 0

Lab 922 first reported 0

Lab 6016 first reported 100

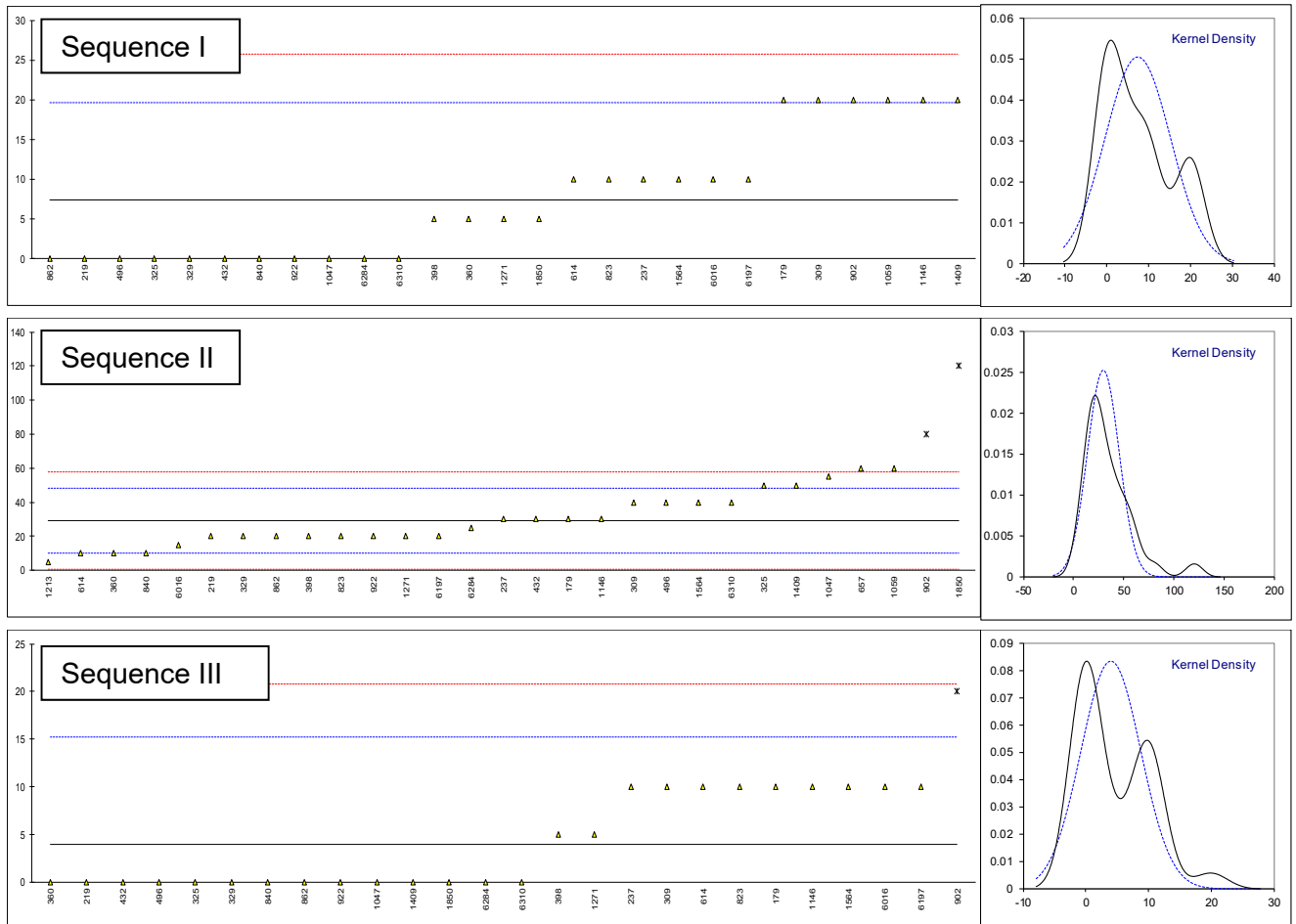
*) see paragraph 4.1 for explanation for the choice of version 2013e1 for evaluation

**) Lab 6016: Sample for foaming was put in ultrasonic bath, homogenized. Without stirring, 200ml of sample decanted into a beaker, heated to 50°C and then cooled to 25°C (ambient temperature)

Lab 6284: Sample was pre heated at 50°C for 10 mins prior to foaming characteristics testing

Sequence I -stone or metal diffuser:

| | Sequence 1 | | Sequence II | |
|--------------------|---------------------|---------------------|---------------------|---------------------|
| | stone diffuser only | metal diffuser only | stone diffuser only | metal diffuser only |
| normality | OK | OK | not OK | OK |
| n | 13 | 13 | 13 | 12 |
| outliers | 0 | 0 | 0 | 0 |
| mean (n) | 3.85 | 11.54 | 23.85 | 35.00 |
| st.dev. (n) | 4.160 | 8.987 | 13.409 | 14.460 |
| R(calc.) | 11.65 | 25.16 | 37.55 | 40.49 |
| st.dev.(D892:13e1) | 6.128 | 6.128 | 9.562 | 9.562 |
| R(D892:13e1) | 15.59 | 18.98 | 24.394 | 29.300 |



Determination of Foam Stability, 10 min settling point on sample #20075; results in mL

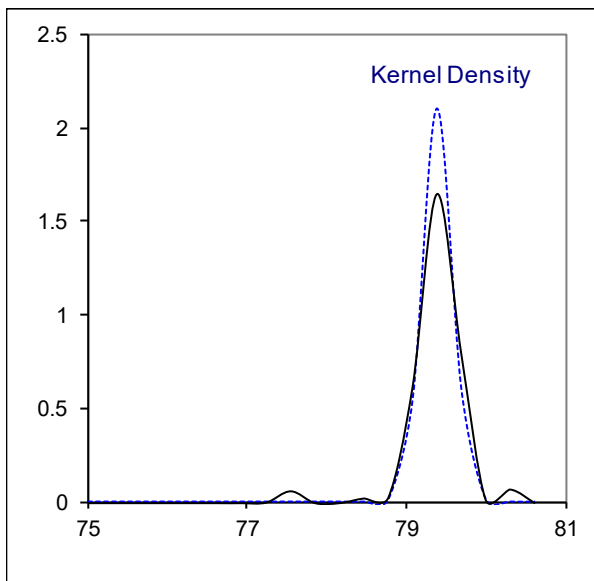
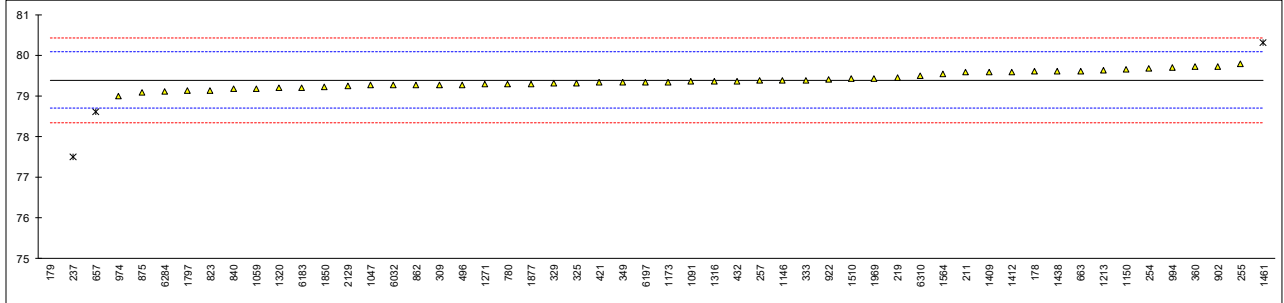
| lab | method | Seq. I | mark | z(targ) | Seq. II | mark | z(targ) | Seq. III | mark | z(targ) |
|------|---------|--------|------|---------|---------|------|---------|----------|------|---------|
| 178 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 179 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 211 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 219 | | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 237 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 254 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 255 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 257 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 309 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 325 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 329 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 333 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 339 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 349 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 360 | ISO6247 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 398 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 421 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 432 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 496 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 614 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 621 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 633 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 634 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 657 | D892 | NIL | | ---- | NIL | | ---- | NIL | | ---- |
| 663 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 780 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 823 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 840 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 862 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 875 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 902 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 912 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 913 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 922 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 962 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 963 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 974 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 994 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1011 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1017 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1047 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 1059 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 1091 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1146 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 1150 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1173 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1213 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1235 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1271 | ISO6247 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 1316 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1320 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1409 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 1412 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1438 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1461 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1510 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1564 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 1748 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1797 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1850 | ISO6247 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 1877 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1969 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 2129 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6016 | | ---- | | ---- | 0 | | ---- | ---- | | ---- |
| 6032 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6183 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6197 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 6253 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6284 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 6310 | D892 | 0 | | ---- | 0 | | ---- | 0 | | ---- |
| 6317 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6320 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6324 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |

| lab | method | Seq. I | mark | z(targ) | Seq. II | mark | z(targ) | Seq. III | mark | z(targ) |
|-----|----------|--------|------|---------|---------|------|---------|----------|------|---------|
| | n | 26 | | | 27 | | | 26 | | |
| | mean (n) | 0 | | | 0 | | | 0 | | |

Determination of Kinematic Viscosity at 40°C on sample #20075; results in mm²/s

| lab | method | value | mark | z(targ) | remarks |
|------|---------------------|---------|-----------|---------|------------------------|
| 178 | D445 | 79.6 | | 0.62 | |
| 179 | D445 | 2.93 | R(0.01) | -221.04 | |
| 211 | D445 | 79.58 | | 0.56 | |
| 219 | D7279 corr. to D445 | 79.44 | | 0.16 | |
| 237 | D445 | 77.49 | R(0.01) | -5.48 | |
| 254 | D445 | 79.68 | | 0.85 | |
| 255 | D7279 corr. to D445 | 79.78 | | 1.14 | |
| 257 | D7279 corr. to D445 | 79.38 | | -0.01 | |
| 309 | D445 | 79.27 | | -0.33 | |
| 325 | D445 | 79.32 | | -0.19 | |
| 329 | D445 | 79.31 | | -0.22 | |
| 333 | D445 | 79.39 | | 0.02 | |
| 339 | | ---- | | ---- | |
| 349 | D445 | 79.34 | | -0.13 | |
| 360 | ISO3104 | 79.727 | | 0.99 | |
| 398 | | ---- | | ---- | |
| 421 | ISO3104 | 79.33 | | -0.16 | |
| 432 | D445 | 79.36 | | -0.07 | |
| 496 | D445 | 79.272 | | -0.33 | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D445 | 78.61 | R(0.01) | -2.24 | |
| 663 | D445 | 79.6002 | | 0.62 | |
| 780 | D445 | 79.29 | | -0.27 | |
| 823 | D445 | 79.14 | | -0.71 | |
| 840 | D445 | 79.174 | | -0.61 | |
| 862 | D445 | 79.26 | | -0.36 | |
| 875 | D445 | 79.09 | | -0.85 | |
| 902 | D445 | 79.73 | | 1.00 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D445 | 79.40 | | 0.04 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D445 | 79.00 | | -1.11 | |
| 994 | D445 | 79.69 | | 0.88 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | ISO3104 | 79.256 | | -0.37 | |
| 1059 | ISO3104 | 79.18 | | -0.59 | |
| 1091 | D445 | 79.35 | | -0.10 | |
| 1146 | D445 | 79.381 | | -0.01 | |
| 1150 | ISO3104 | 79.6591 | | 0.79 | |
| 1173 | IP71 | 79.342 | | -0.12 | |
| 1213 | D445 | 79.62 | | 0.68 | |
| 1235 | | ---- | | ---- | |
| 1271 | ISO3104 | 79.287 | | -0.28 | |
| 1316 | ISO3104 | 79.35 | | -0.10 | |
| 1320 | ISO3104 | 79.20 | | -0.53 | |
| 1409 | D445 | 79.58 | | 0.56 | |
| 1412 | D445 | 79.59 | | 0.59 | |
| 1438 | D445 | 79.6 | | 0.62 | |
| 1461 | ISO3104 | 80.2979 | C,R(0.01) | 2.64 | first reported 80.7192 |
| 1510 | D445 | 79.43 | | 0.13 | |
| 1564 | D445 | 79.53 | | 0.42 | |
| 1748 | | ---- | | ---- | |
| 1797 | ISO3104 | 79.12 | | -0.77 | |
| 1850 | ISO3104 | 79.22 | | -0.48 | |
| 1877 | D445 | 79.29 | | -0.27 | |
| 1969 | ISO3104 | 79.4358 | | 0.15 | |
| 2129 | D445 | 79.254 | | -0.38 | |
| 6016 | | ---- | | ---- | |
| 6032 | D7279 corr. to D445 | 79.257 | | -0.37 | |
| 6183 | D445 | 79.20 | | -0.53 | |
| 6197 | D445 | 79.34 | | -0.13 | |
| 6253 | | ---- | | ---- | |
| 6284 | D445 | 79.1127 | | -0.79 | |
| 6310 | D7279 corr. to D445 | 79.5 | | 0.33 | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

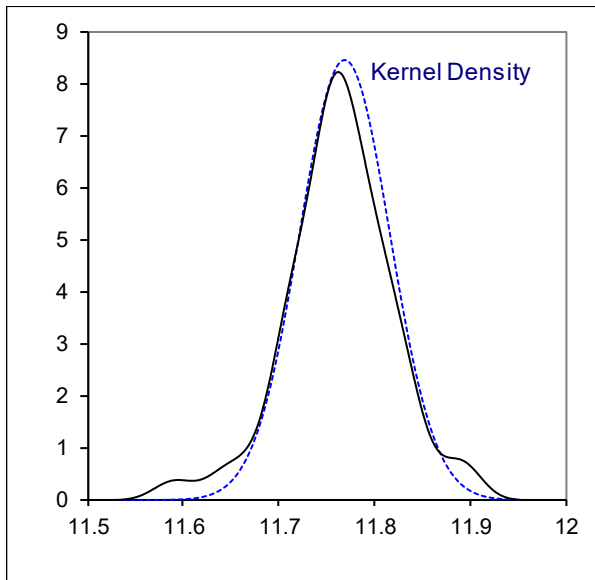
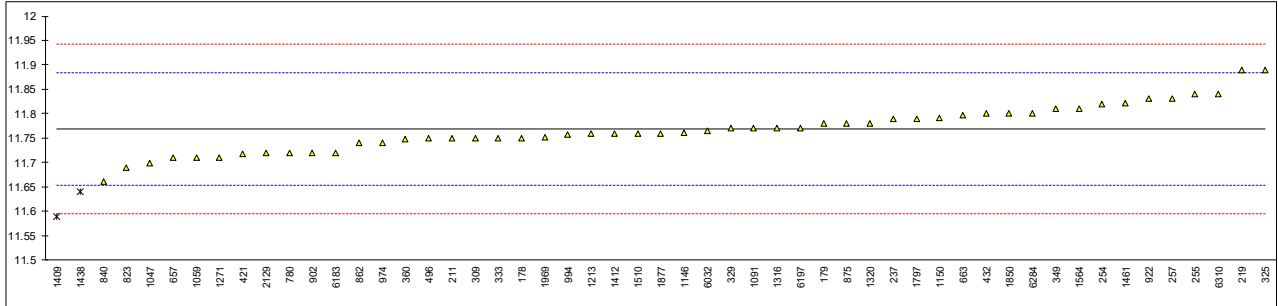
| | |
|------------------|--------|
| normality | OK |
| n | 50 |
| outliers | 4 |
| mean (n) | 79.385 |
| st.dev. (n) | 0.1898 |
| R(calc.) | 0.531 |
| st.dev.(D445:19) | 0.3459 |
| R(D445:19) | 0.968 |



Determination of Kinematic Viscosity at 100°C on sample #20075; results in mm²/s

| lab | method | value | mark | z(targ) | remarks |
|------|---------------------|---------|------------|---------|------------------------|
| 178 | D445 | 11.75 | | -0.32 | |
| 179 | D445 | 11.78 | | 0.20 | |
| 211 | D445 | 11.75 | | -0.32 | |
| 219 | D7279 corr. to D445 | 11.89 | | 2.09 | |
| 237 | D445 | 11.79 | | 0.37 | |
| 254 | D445 | 11.82 | | 0.89 | |
| 255 | D7279 corr. to D445 | 11.84 | | 1.23 | |
| 257 | D7279 corr. to D445 | 11.83 | | 1.06 | |
| 309 | D445 | 11.75 | | -0.32 | |
| 325 | D445 | 11.89 | | 2.09 | |
| 329 | D445 | 11.77 | | 0.02 | |
| 333 | D445 | 11.75 | | -0.32 | |
| 339 | | ---- | | ---- | |
| 349 | D445 | 11.81 | | 0.71 | |
| 360 | ISO3104 | 11.748 | | -0.35 | |
| 398 | | ---- | | ---- | |
| 421 | ISO3104 | 11.718 | C | -0.87 | first reported 11.58 |
| 432 | D445 | 11.80 | | 0.54 | |
| 496 | D445 | 11.749 | | -0.34 | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D445 | 11.71 | | -1.01 | |
| 663 | D445 | 11.7967 | | 0.49 | |
| 780 | D445 | 11.72 | | -0.84 | |
| 823 | ISO3104 | 11.69 | | -1.35 | |
| 840 | D445 | 11.661 | | -1.85 | |
| 862 | D445 | 11.74 | | -0.49 | |
| 875 | D445 | 11.78 | | 0.20 | |
| 902 | D445 | 11.72 | | -0.84 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D445 | 11.83 | | 1.06 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D445 | 11.74 | C | -0.49 | first reported 11.53 |
| 994 | D445 | 11.758 | | -0.18 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | ISO3104 | 11.698 | | -1.22 | |
| 1059 | ISO3104 | 11.71 | | -1.01 | |
| 1091 | D445 | 11.77 | | 0.02 | |
| 1146 | D445 | 11.761 | | -0.13 | |
| 1150 | ISO3104 | 11.7904 | | 0.38 | |
| 1173 | | ---- | | ---- | |
| 1213 | D445 | 11.76 | | -0.15 | |
| 1235 | | ---- | | ---- | |
| 1271 | ISO3104 | 11.710 | | -1.01 | |
| 1316 | ISO3104 | 11.77 | | 0.02 | |
| 1320 | ISO3104 | 11.78 | | 0.20 | |
| 1409 | D445 | 11.59 | DG(0.05) | -3.08 | |
| 1412 | D445 | 11.76 | | -0.15 | |
| 1438 | D445 | 11.64 | C,DG(0.05) | -2.22 | first reported 11.6 |
| 1461 | ISO3104 | 11.8213 | | 0.91 | |
| 1510 | D445 | 11.76 | | -0.15 | |
| 1564 | D445 | 11.81 | | 0.71 | |
| 1748 | | ---- | | ---- | |
| 1797 | ISO3104 | 11.79 | | 0.37 | |
| 1850 | ISO3104 | 11.80 | | 0.54 | |
| 1877 | D445 | 11.76 | | -0.15 | |
| 1969 | ISO3104 | 11.7517 | | -0.29 | |
| 2129 | D445 | 11.719 | | -0.85 | |
| 6016 | | ---- | | ---- | |
| 6032 | D7279 corr. to D445 | 11.764 | | -0.08 | |
| 6183 | D445 | 11.72 | | -0.84 | |
| 6197 | D445 | 11.77 | | 0.02 | |
| 6253 | | ---- | | ---- | |
| 6284 | D445 | 11.8003 | C | 0.55 | first reported 11.5937 |
| 6310 | D7279 corr. to D445 | 11.84 | | 1.23 | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

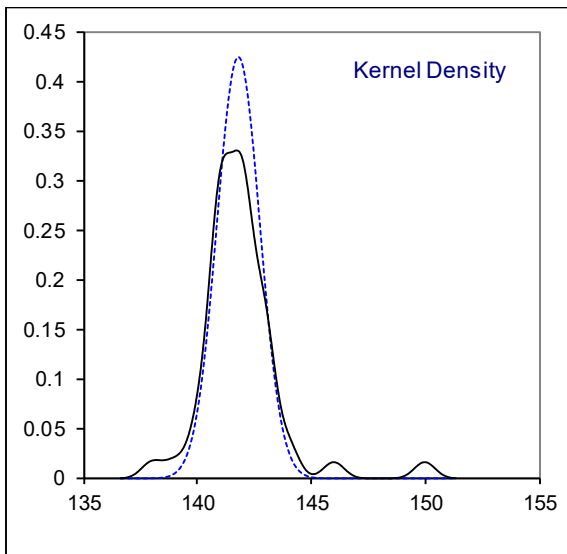
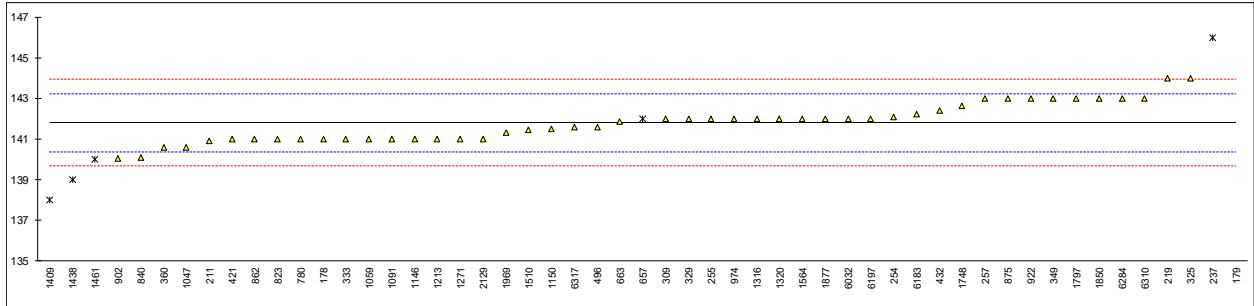
| | |
|------------------|--------|
| normality | OK |
| n | 51 |
| outliers | 2 |
| mean (n) | 11.769 |
| st.dev. (n) | 0.0472 |
| R(calc.) | 0.132 |
| st.dev.(D445:19) | 0.0580 |
| R(D445:19) | 0.162 |



Determination of Viscosity Index on sample #20075;

| lab | method | value | mark | z(targ) | remarks |
|------|---------|---------|------|---------|---|
| 178 | D2270 | 141 | | -1.13 | |
| 179 | D2270 | 3917 | ex | 5285.27 | test result excluded, outlier in KV 40°C |
| 211 | D2270 | 140.9 | | -1.27 | |
| 219 | D2270 | 144 | | 3.07 | |
| 237 | D2270 | 146 | ex | 5.87 | test result excluded, outlier in KV 40°C |
| 254 | D2270 | 142.09 | | 0.40 | |
| 255 | D2270 | 142 | | 0.27 | |
| 257 | D2270 | 143 | | 1.67 | |
| 309 | D2270 | 142 | | 0.27 | |
| 325 | D2270 | 144 | | 3.07 | |
| 329 | D2270 | 142 | | 0.27 | |
| 333 | D2270 | 141 | | -1.13 | |
| 339 | | ---- | | ---- | |
| 349 | D2270 | 143 | | 1.67 | |
| 360 | ISO2909 | 140.6 | | -1.69 | |
| 398 | | ---- | | ---- | |
| 421 | ISO2909 | 141 | | -1.13 | |
| 432 | D2270 | 142.4 | | 0.83 | |
| 496 | D2270 | 141.6 | | -0.29 | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D2270 | 142 | ex | 0.27 | test result excluded, outlier in KV 40°C |
| 663 | D2270 | 141.87 | | 0.09 | |
| 780 | D2270 | 141 | | -1.13 | |
| 823 | D2270 | 141 | | -1.13 | |
| 840 | D2270 | 140.1 | | -2.39 | |
| 862 | D2270 | 141 | | -1.13 | |
| 875 | D2270 | 143 | | 1.67 | |
| 902 | D2270 | 140.05 | | -2.46 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D2270 | 143 | | 1.67 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D2270 | 142 | C | 0.27 | first reported 138 |
| 994 | | ---- | | ---- | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | ISO2909 | 140.6 | | -1.69 | |
| 1059 | ISO2909 | 141 | | -1.13 | |
| 1091 | D2270 | 141 | | -1.13 | |
| 1146 | D2270 | 141 | | -1.13 | |
| 1150 | ISO2909 | 141.48 | | -0.46 | |
| 1173 | | ---- | | ---- | |
| 1213 | D2270 | 141 | | -1.13 | |
| 1235 | | ---- | | ---- | |
| 1271 | ISO2909 | 141 | | -1.13 | |
| 1316 | D2270 | 142 | | 0.27 | |
| 1320 | D2270 | 142 | | 0.27 | |
| 1409 | D2270 | 138 | ex | -5.33 | test result excluded, outlier in KV 100°C |
| 1412 | | ---- | | ---- | |
| 1438 | | 139 | ex | -3.93 | test result excluded, outlier in KV 100°C |
| 1461 | ISO2909 | 140 | ex | -2.53 | test result excluded, outlier in KV 40°C |
| 1510 | D2270 | 141.467 | | -0.47 | |
| 1564 | D2270 | 142 | | 0.27 | |
| 1748 | D2270 | 142.63 | | 1.15 | |
| 1797 | ISO2909 | 143 | | 1.67 | |
| 1850 | ISO2909 | 143 | | 1.67 | |
| 1877 | D2270 | 142 | | 0.27 | |
| 1969 | ISO2909 | 141.29 | | -0.72 | |
| 2129 | D2270 | 141.0 | | -1.13 | |
| 6016 | | ---- | | ---- | |
| 6032 | D2270 | 142 | | 0.27 | |
| 6183 | D2270 | 142.2 | | 0.55 | |
| 6197 | D2270 | 142 | | 0.27 | |
| 6253 | | ---- | | ---- | |
| 6284 | D2270 | 143 | C | 1.67 | first reported 138.89 |
| 6310 | D2270 | 143 | | 1.67 | |
| 6317 | D2270 | 141.57 | | -0.33 | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

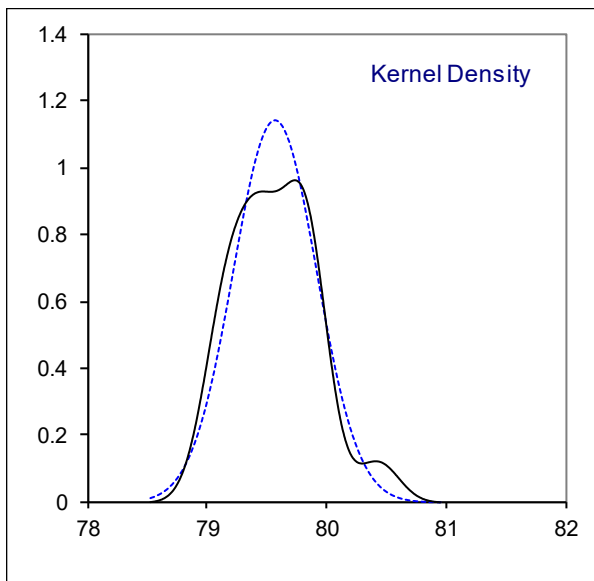
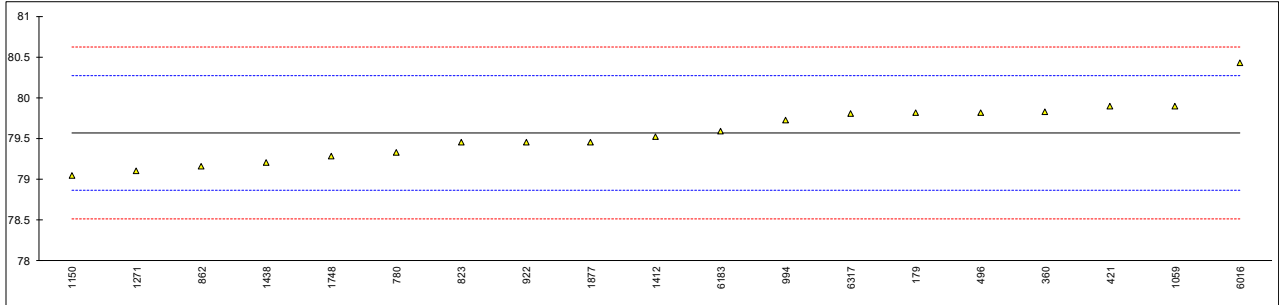
| | |
|-------------------|---------|
| normality | OK |
| n | 47 |
| outliers | 0+(6ex) |
| mean (n) | 141.81 |
| st.dev. (n) | 0.942 |
| R(calc.) | 2.64 |
| st.dev.(D2270:10) | 0.714 |
| R(D2270:10) | 2 |



Determination of Viscosity Stabinger at 40°C on sample #20075; results in mm²/s

| lab | method | value | mark | z(targ) | remarks |
|------|--------|---------|------|---------|---------|
| 178 | | ---- | | ---- | |
| 179 | D7042 | 79.81 | | 0.69 | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | | ---- | | ---- | |
| 254 | | ---- | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | ---- | | ---- | |
| 325 | | ---- | | ---- | |
| 329 | | ---- | | ---- | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | | ---- | | ---- | |
| 360 | D7042 | 79.828 | | 0.75 | |
| 398 | | ---- | | ---- | |
| 421 | D7042 | 79.89 | | 0.92 | |
| 432 | | ---- | | ---- | |
| 496 | D7042 | 79.813 | | 0.70 | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | | ---- | | ---- | |
| 663 | | ---- | | ---- | |
| 780 | D7042 | 79.33 | | -0.68 | |
| 823 | D7042 | 79.45 | | -0.33 | |
| 840 | | ---- | | ---- | |
| 862 | D7042 | 79.162 | | -1.16 | |
| 875 | | ---- | | ---- | |
| 902 | | ---- | | ---- | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D7042 | 79.45 | | -0.33 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | | ---- | | ---- | |
| 994 | D7042 | 79.72 | | 0.44 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | ---- | | ---- | |
| 1059 | D7042 | 79.90 | | 0.95 | |
| 1091 | | ---- | | ---- | |
| 1146 | | ---- | | ---- | |
| 1150 | D7042 | 79.0445 | | -1.49 | |
| 1173 | | ---- | | ---- | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | D7042 | 79.107 | | -1.31 | |
| 1316 | | ---- | | ---- | |
| 1320 | | ---- | | ---- | |
| 1409 | | ---- | | ---- | |
| 1412 | D7042 | 79.52 | | -0.13 | |
| 1438 | | 79.2 | | -1.05 | |
| 1461 | | ---- | | ---- | |
| 1510 | | ---- | | ---- | |
| 1564 | | ---- | | ---- | |
| 1748 | D7042 | 79.281 | | -0.82 | |
| 1797 | | ---- | | ---- | |
| 1850 | | ---- | | ---- | |
| 1877 | D7042 | 79.45 | | -0.33 | |
| 1969 | | ---- | | ---- | |
| 2129 | | ---- | | ---- | |
| 6016 | D7042 | 80.431 | | 2.47 | |
| 6032 | | ---- | | ---- | |
| 6183 | D7042 | 79.59 | | 0.07 | |
| 6197 | | ---- | | ---- | |
| 6253 | | ---- | | ---- | |
| 6284 | | ---- | | ---- | |
| 6310 | | ---- | | ---- | |
| 6317 | D7042 | 79.8 | | 0.67 | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

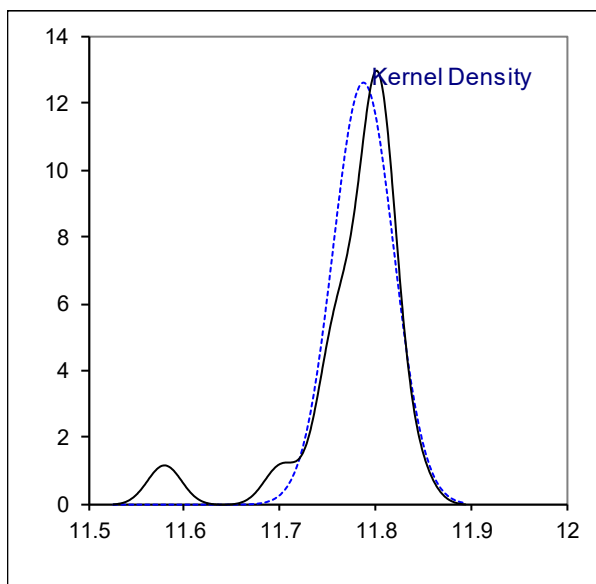
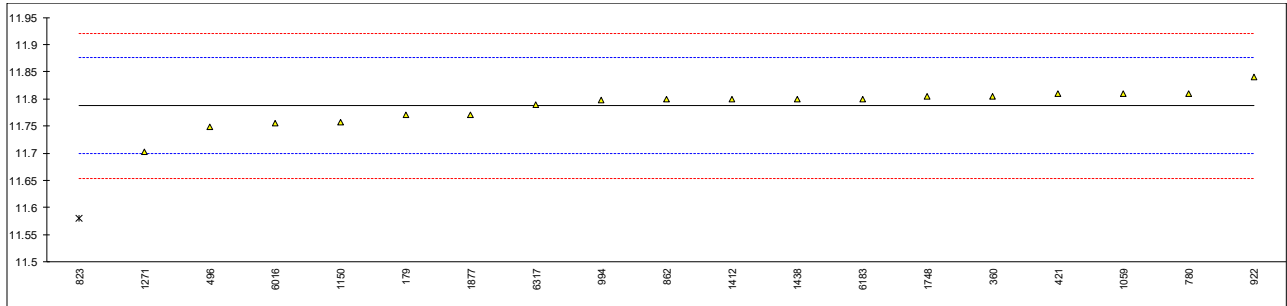
| | |
|---------------------|--------|
| normality | OK |
| n | 19 |
| outliers | 0 |
| mean (n) | 79.567 |
| st.dev. (n) | 0.3490 |
| R(calc.) | 0.977 |
| st.dev.(D7042:19e1) | 0.3500 |
| R(D7042:19e1) | 0.980 |



Determination of Viscosity Stabinger at 100°C on sample #20075; results in mm²/s

| lab | method | value | mark | z(targ) | remarks |
|------|--------|---------|-----------|---------|-----------------------|
| 178 | | ---- | | ---- | |
| 179 | D7042 | 11.77 | | -0.39 | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | | ---- | | ---- | |
| 254 | | ---- | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | ---- | | ---- | |
| 325 | | ---- | | ---- | |
| 329 | | ---- | | ---- | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | | ---- | | ---- | |
| 360 | D7042 | 11.805 | | 0.40 | |
| 398 | | ---- | | ---- | |
| 421 | D7042 | 11.81 | | 0.52 | |
| 432 | | ---- | | ---- | |
| 496 | D7042 | 11.749 | | -0.86 | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | | ---- | | ---- | |
| 663 | | ---- | | ---- | |
| 780 | D7042 | 11.81 | | 0.52 | |
| 823 | D7042 | 11.58 | C,D(0.01) | -4.67 | first reported 11.44 |
| 840 | | ---- | | ---- | |
| 862 | D7042 | 11.80 | | 0.29 | |
| 875 | | ---- | | ---- | |
| 902 | | ---- | | ---- | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D7042 | 11.84 | | 1.19 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | | ---- | | ---- | |
| 994 | D7042 | 11.797 | | 0.22 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | ---- | | ---- | |
| 1059 | D7042 | 11.81 | | 0.52 | |
| 1091 | | ---- | | ---- | |
| 1146 | | ---- | | ---- | |
| 1150 | D7042 | 11.7573 | | -0.67 | |
| 1173 | | ---- | | ---- | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | D7042 | 11.702 | | -1.92 | |
| 1316 | | ---- | | ---- | |
| 1320 | | ---- | | ---- | |
| 1409 | | ---- | | ---- | |
| 1412 | D7042 | 11.80 | | 0.29 | |
| 1438 | | 11.8 | | 0.29 | |
| 1461 | | ---- | | ---- | |
| 1510 | | ---- | | ---- | |
| 1564 | | ---- | | ---- | |
| 1748 | D7042 | 11.804 | | 0.38 | |
| 1797 | | ---- | | ---- | |
| 1850 | | ---- | | ---- | |
| 1877 | D7042 | 11.77 | | -0.39 | |
| 1969 | | ---- | | ---- | |
| 2129 | | ---- | | ---- | |
| 6016 | D7042 | 11.7545 | C | -0.74 | first reported 11.931 |
| 6032 | | ---- | | ---- | |
| 6183 | D7042 | 11.80 | | 0.29 | |
| 6197 | | ---- | | ---- | |
| 6253 | | ---- | | ---- | |
| 6284 | | ---- | | ---- | |
| 6310 | | ---- | | ---- | |
| 6317 | D7042 | 11.7895 | | 0.05 | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

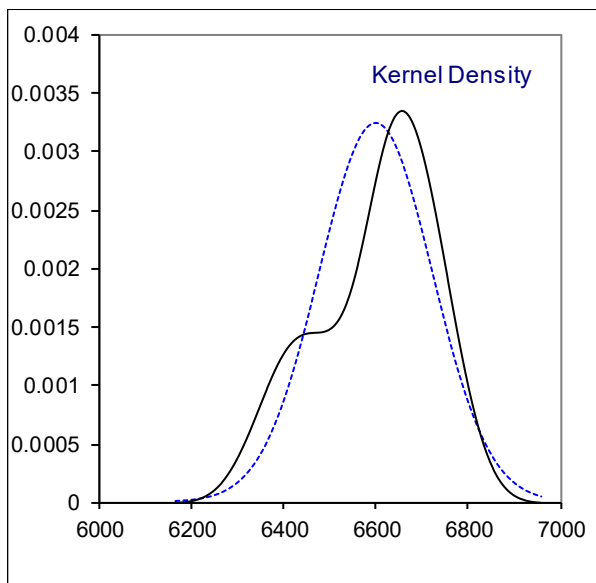
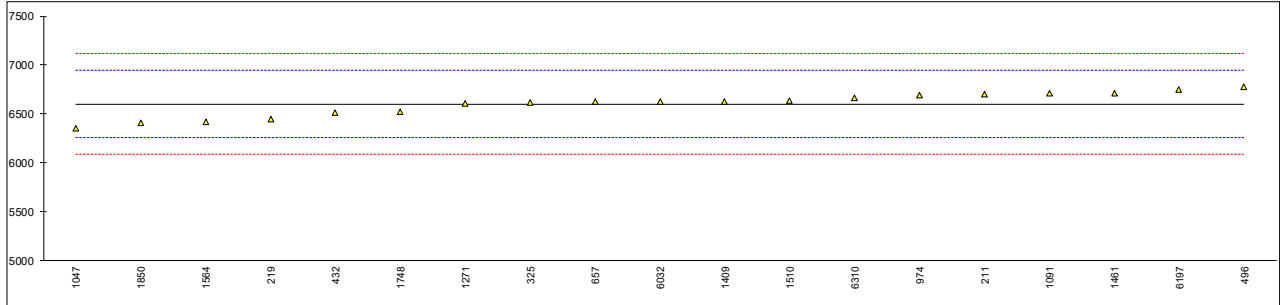
| | |
|---------------------|---------|
| normality | suspect |
| n | 18 |
| outliers | 1 |
| mean (n) | 11.787 |
| st.dev. (n) | 0.0316 |
| R(calc.) | 0.088 |
| st.dev.(D7042:19e1) | 0.0443 |
| R(D7042:19e1) | 0.124 |



Determination of Viscosity Apparent (CCS) at -25°C on sample #20075; results in mPa·s

| lab | method | value | mark | z(targ) | remarks |
|------|----------|-------|------|---------|---------------------|
| 178 | | ---- | | ---- | |
| 179 | | ---- | | ---- | |
| 211 | D5293 | 6700 | | 0.58 | |
| 219 | D5293 | 6450 | | -0.88 | |
| 237 | | ---- | | ---- | |
| 254 | | ---- | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | ---- | | ---- | |
| 325 | D5293 | 6620 | | 0.11 | |
| 329 | | ---- | | ---- | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | | ---- | | ---- | |
| 360 | | ---- | | ---- | |
| 398 | | ---- | | ---- | |
| 421 | | ---- | | ---- | |
| 432 | D5293 | 6511 | | -0.52 | |
| 496 | D5293 | 6776 | | 1.02 | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D5293 | 6623 | | 0.13 | |
| 663 | | ---- | | ---- | |
| 780 | | ---- | | ---- | |
| 823 | | ---- | | ---- | |
| 840 | | ---- | | ---- | |
| 862 | | ---- | | ---- | |
| 875 | | ---- | | ---- | |
| 902 | | ---- | | ---- | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | | ---- | | ---- | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D5293 | 6694 | | 0.54 | |
| 994 | | ---- | | ---- | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | D5293 | 6350 | C | -1.46 | first reported 2780 |
| 1059 | | ---- | | ---- | |
| 1091 | D5293 | 6710 | | 0.64 | |
| 1146 | | ---- | | ---- | |
| 1150 | | ---- | | ---- | |
| 1173 | | ---- | | ---- | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | D5293 | 6611 | | 0.06 | |
| 1316 | | ---- | | ---- | |
| 1320 | | ---- | | ---- | |
| 1409 | D5293 | 6627 | | 0.15 | |
| 1412 | | ---- | | ---- | |
| 1438 | | ---- | | ---- | |
| 1461 | In house | 6711 | | 0.64 | |
| 1510 | D5293 | 6640 | | 0.23 | |
| 1564 | D5293 | 6423 | | -1.03 | |
| 1748 | D5293 | 6520 | | -0.47 | |
| 1797 | | ---- | | ---- | |
| 1850 | D5293 | 6410 | | -1.11 | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | | ---- | | ---- | |
| 6016 | | ---- | | ---- | |
| 6032 | D5293 | 6626 | | 0.15 | |
| 6183 | | ---- | | ---- | |
| 6197 | D5293 | 6749 | | 0.86 | |
| 6253 | | ---- | | ---- | |
| 6284 | | ---- | | ---- | |
| 6310 | D5293 | 6661 | | 0.35 | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

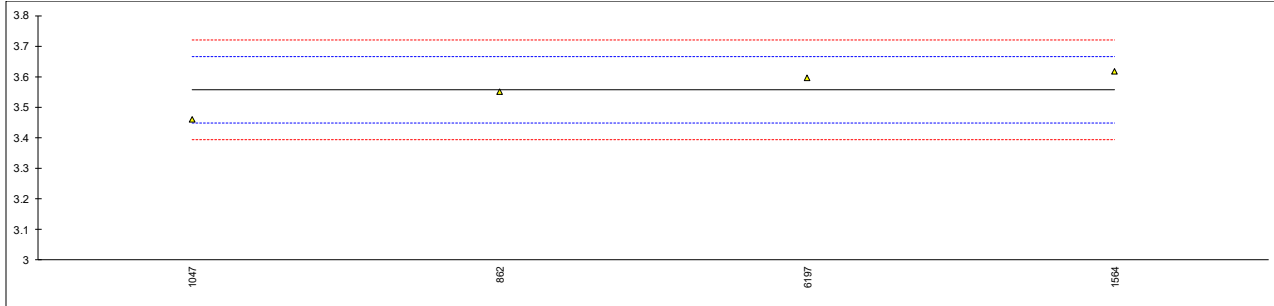
| | |
|--------------------|--------|
| normality | OK |
| n | 19 |
| outliers | 0 |
| mean (n) | 6600.6 |
| st.dev. (n) | 122.69 |
| R(calc.) | 343.5 |
| st.dev.(D5293:17a) | 172.09 |
| R(D5293:17a) | 481.8 |



Determination of Viscosity HTHS by Tapered Bearing Simulator on sample #20075; results in mPa·s

| lab | method | value | mark | z(targ) | remarks |
|------|--------|-------|------|---------|---------|
| 178 | | ---- | | ---- | |
| 179 | | ---- | | ---- | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | | ---- | | ---- | |
| 254 | | ---- | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | ---- | | ---- | |
| 325 | | ---- | | ---- | |
| 329 | | ---- | | ---- | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | | ---- | | ---- | |
| 360 | | ---- | | ---- | |
| 398 | | ---- | | ---- | |
| 421 | | ---- | | ---- | |
| 432 | | ---- | | ---- | |
| 496 | | ---- | | ---- | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | | ---- | | ---- | |
| 663 | | ---- | | ---- | |
| 780 | | ---- | | ---- | |
| 823 | | ---- | | ---- | |
| 840 | | ---- | | ---- | |
| 862 | D4741 | 3.55 | | -0.11 | |
| 875 | | ---- | | ---- | |
| 902 | | ---- | | ---- | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | | ---- | | ---- | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | | ---- | | ---- | |
| 994 | | ---- | | ---- | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | D4741 | 3.46 | | -1.76 | |
| 1059 | | ---- | | ---- | |
| 1091 | | ---- | | ---- | |
| 1146 | | ---- | | ---- | |
| 1150 | | ---- | | ---- | |
| 1173 | | ---- | | ---- | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | | ---- | | ---- | |
| 1316 | | ---- | | ---- | |
| 1320 | | ---- | | ---- | |
| 1409 | | ---- | | ---- | |
| 1412 | | ---- | | ---- | |
| 1438 | | ---- | | ---- | |
| 1461 | | ---- | | ---- | |
| 1510 | | ---- | | ---- | |
| 1564 | D4683 | 3.618 | | 1.13 | |
| 1748 | | ---- | | ---- | |
| 1797 | | ---- | | ---- | |
| 1850 | | ---- | | ---- | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | | ---- | | ---- | |
| 6016 | | ---- | | ---- | |
| 6032 | | ---- | | ---- | |
| 6183 | | ---- | | ---- | |
| 6197 | D5481 | 3.597 | | 0.75 | |
| 6253 | | ---- | | ---- | |
| 6284 | | ---- | | ---- | |
| 6310 | | ---- | | ---- | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

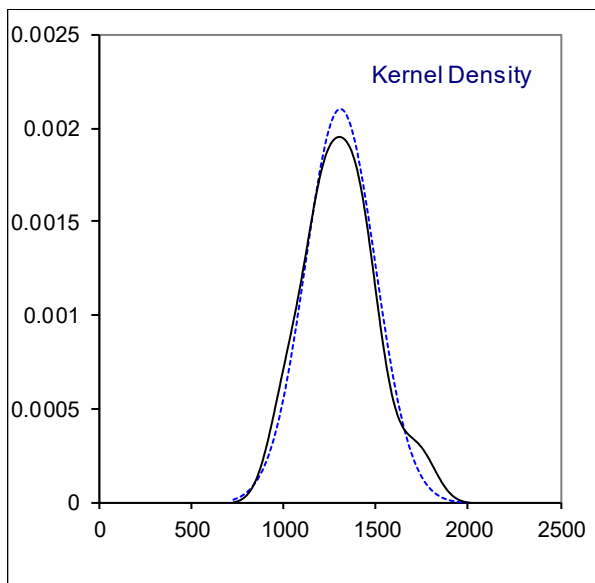
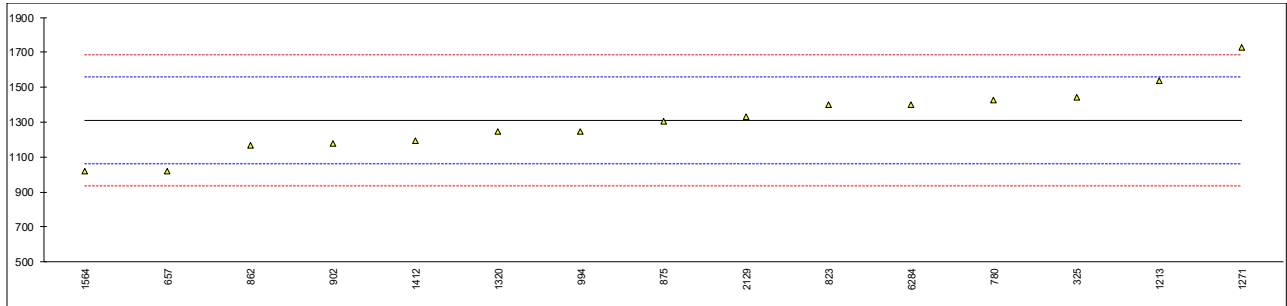
| | |
|-------------------|---------|
| normality | unknown |
| n | 4 |
| outliers | 0 |
| mean (n) | 3.556 |
| st.dev. (n) | 0.0702 |
| R(calc.) | 0.197 |
| st.dev.(D4683:17) | 0.0546 |
| R(D4683:17) | 0.153 |



Determination of Nitrogen on sample #20075; results in mg/kg

| lab | method | value | mark | z(targ) | remarks |
|------|--------|-------|------|---------|---------------------|
| 178 | | ---- | | ---- | |
| 179 | | ---- | | ---- | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | | ---- | | ---- | |
| 254 | | ---- | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | ---- | | ---- | |
| 325 | D5762 | 1441 | | 1.05 | |
| 329 | | ---- | | ---- | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | | ---- | | ---- | |
| 360 | | ---- | | ---- | |
| 398 | | ---- | | ---- | |
| 421 | | ---- | | ---- | |
| 432 | | ---- | | ---- | |
| 496 | | ---- | | ---- | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D5762 | 1021 | | -2.32 | |
| 663 | | ---- | | ---- | |
| 780 | D3228 | 1426 | | 0.93 | |
| 823 | D5762 | 1400 | | 0.72 | |
| 840 | | ---- | | ---- | |
| 862 | D5762 | 1168 | | -1.14 | |
| 875 | D5762 | 1306 | | -0.03 | |
| 902 | D5762 | 1179 | | -1.05 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | | ---- | | ---- | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | | ---- | | ---- | |
| 994 | D5762 | 1249 | | -0.49 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | ---- | | ---- | |
| 1059 | | ---- | | ---- | |
| 1091 | | ---- | | ---- | |
| 1146 | | ---- | | ---- | |
| 1150 | | ---- | | ---- | |
| 1173 | | ---- | | ---- | |
| 1213 | D5762 | 1539 | | 1.84 | |
| 1235 | | ---- | | ---- | |
| 1271 | D3228 | 1730 | | 3.37 | |
| 1316 | | ---- | | ---- | |
| 1320 | D5762 | 1248 | | -0.50 | |
| 1409 | | ---- | | ---- | |
| 1412 | D5762 | 1192 | | -0.95 | |
| 1438 | | ---- | | ---- | |
| 1461 | | ---- | | ---- | |
| 1510 | | ---- | | ---- | |
| 1564 | D5762 | 1020 | | -2.33 | |
| 1748 | | ---- | | ---- | |
| 1797 | | ---- | | ---- | |
| 1850 | | ---- | | ---- | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | D3228 | 1333 | | 0.18 | |
| 6016 | | ---- | | ---- | |
| 6032 | | ---- | | ---- | |
| 6183 | | ---- | | ---- | |
| 6197 | | ---- | | ---- | |
| 6253 | | ---- | | ---- | |
| 6284 | D3228 | 1400 | C | 0.72 | first reported 2800 |
| 6310 | | ---- | | ---- | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

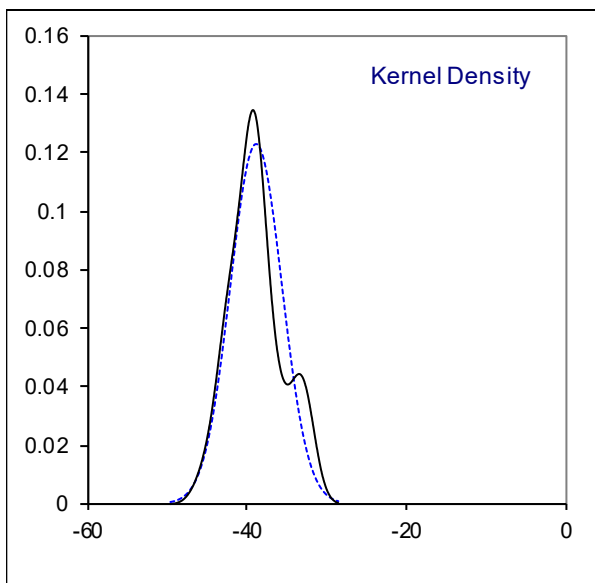
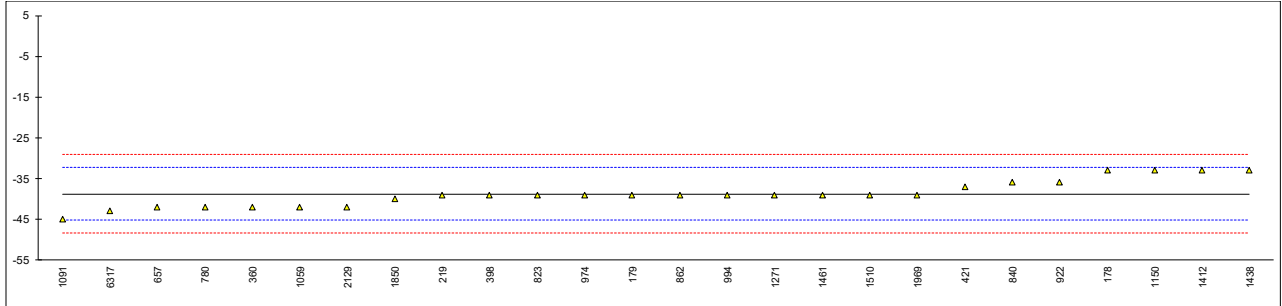
| | |
|--------------------|---------|
| normality | OK |
| n | 15 |
| outliers | 0 |
| mean (n) | 1310.13 |
| st.dev. (n) | 189.480 |
| R(calc.) | 530.54 |
| st.dev.(D5762:18a) | 124.463 |
| R(D5762:18a) | 348.50 |



Determination of Pour Point, Manual on sample #20075; results in °C

| lab | method | value | mark | z(targ) | remarks |
|------|---------|-------|------|---------|---------|
| 178 | D97 | -33 | | 1.79 | |
| 179 | D97 | -39 | | -0.07 | |
| 211 | | ---- | | ---- | |
| 219 | D97 | -39 | | -0.07 | |
| 237 | | ---- | | ---- | |
| 254 | D97 | <-24 | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | ---- | | ---- | |
| 325 | | ---- | | ---- | |
| 329 | | ---- | | ---- | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | | ---- | | ---- | |
| 360 | ISO3016 | -42 | | -1.01 | |
| 398 | D97 | -39 | | -0.07 | |
| 421 | ISO3016 | -37 | | 0.55 | |
| 432 | | ---- | | ---- | |
| 496 | | ---- | | ---- | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D97 | -42 | | -1.01 | |
| 663 | D97 | <-36 | | ---- | |
| 780 | D97 | -42 | | -1.01 | |
| 823 | D97 | -39 | | -0.07 | |
| 840 | D97 | -36 | | 0.86 | |
| 862 | D97 | -39 | | -0.07 | |
| 875 | | ---- | | ---- | |
| 902 | | ---- | | ---- | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D97 | -36 | | 0.86 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D97 | -39 | | -0.07 | |
| 994 | D97 | -39 | | -0.07 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | ---- | | ---- | |
| 1059 | ISO3016 | -42 | | -1.01 | |
| 1091 | ISO3016 | -45 | | -1.94 | |
| 1146 | | ---- | | ---- | |
| 1150 | ISO3016 | -33 | | 1.79 | |
| 1173 | | ---- | | ---- | |
| 1213 | D97 | < -42 | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | ISO3016 | -39 | | -0.07 | |
| 1316 | | ---- | | ---- | |
| 1320 | | ---- | | ---- | |
| 1409 | | ---- | | ---- | |
| 1412 | D97 | -33 | | 1.79 | |
| 1438 | | -33 | | 1.79 | |
| 1461 | ISO3016 | -39 | | -0.07 | |
| 1510 | D97 | -39 | | -0.07 | |
| 1564 | | ---- | | ---- | |
| 1748 | | ---- | | ---- | |
| 1797 | | ---- | | ---- | |
| 1850 | ISO3016 | -40 | | -0.38 | |
| 1877 | | ---- | | ---- | |
| 1969 | ISO3016 | -39 | | -0.07 | |
| 2129 | D97 | -42.0 | | -1.01 | |
| 6016 | | ---- | | ---- | |
| 6032 | | ---- | | ---- | |
| 6183 | | ---- | | ---- | |
| 6197 | | ---- | | ---- | |
| 6253 | | ---- | | ---- | |
| 6284 | | ---- | | ---- | |
| 6310 | | ---- | | ---- | |
| 6317 | D97 | -43 | | -1.32 | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

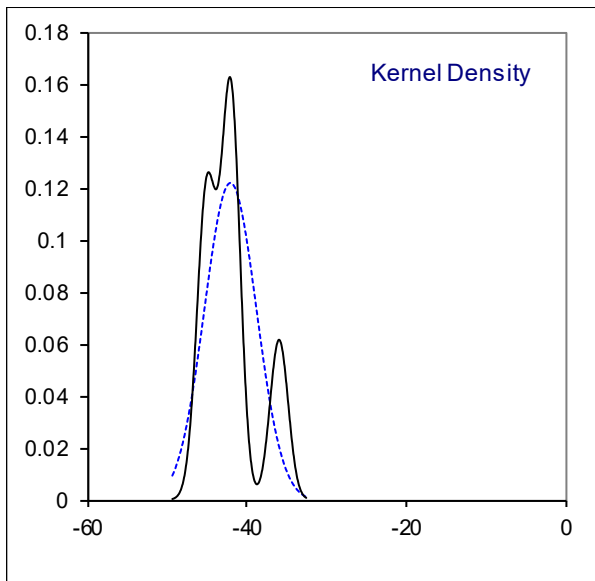
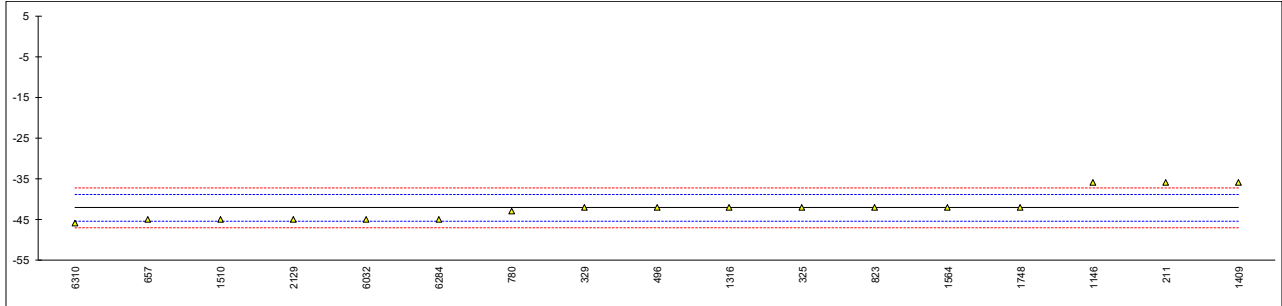
| | |
|------------------|--------|
| normality | OK |
| n | 26 |
| outliers | 0 |
| mean (n) | -38.77 |
| st.dev. (n) | 3.241 |
| R(calc.) | 9.08 |
| st.dev.(D97:17b) | 3.214 |
| R(D97:17b) | 9 |



Determination of Pour Point, Automated, 1°C interval on sample #20075; results in °C

| lab | method | value | mark | z(targ) | remarks |
|------|----------|-------|------|---------|---------|
| 178 | | ---- | | ---- | |
| 179 | | ---- | | ---- | |
| 211 | D5950 | -36 | | 3.81 | |
| 219 | | ---- | | ---- | |
| 237 | | ---- | | ---- | |
| 254 | | ---- | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | ---- | | ---- | |
| 325 | D5950 | -42 | | 0.07 | |
| 329 | D5950 | -42 | | 0.07 | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | | ---- | | ---- | |
| 360 | | ---- | | ---- | |
| 398 | | ---- | | ---- | |
| 421 | | ---- | | ---- | |
| 432 | | ---- | | ---- | |
| 496 | D5950 | -42 | | 0.07 | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D5950 | -45 | | -1.79 | |
| 663 | | ---- | | ---- | |
| 780 | D5950 | -43 | | -0.55 | |
| 823 | D5950 | -42 | | 0.07 | |
| 840 | | ---- | | ---- | |
| 862 | | ---- | | ---- | |
| 875 | | ---- | | ---- | |
| 902 | | ---- | | ---- | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | | ---- | | ---- | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | | ---- | | ---- | |
| 994 | | ---- | | ---- | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | ---- | | ---- | |
| 1059 | | ---- | | ---- | |
| 1091 | | ---- | | ---- | |
| 1146 | In house | -36 | | 3.81 | |
| 1150 | | ---- | | ---- | |
| 1173 | | ---- | | ---- | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | | ---- | | ---- | |
| 1316 | D5950 | -42.0 | | 0.07 | |
| 1320 | | ---- | | ---- | |
| 1409 | D5950 | -36 | | 3.81 | |
| 1412 | | ---- | | ---- | |
| 1438 | | ---- | | ---- | |
| 1461 | | ---- | | ---- | |
| 1510 | D5950 | -45 | | -1.79 | |
| 1564 | D5950 | -42 | | 0.07 | |
| 1748 | D7346 | -42 | | 0.07 | |
| 1797 | | ---- | | ---- | |
| 1850 | | ---- | | ---- | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | D5950 | -45.0 | | -1.79 | |
| 6016 | | ---- | | ---- | |
| 6032 | D5950 | -45 | | -1.79 | |
| 6183 | | ---- | | ---- | |
| 6197 | | ---- | | ---- | |
| 6253 | | ---- | | ---- | |
| 6284 | D5950 | -45 | | -1.79 | |
| 6310 | D5950 | -46 | | -2.42 | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

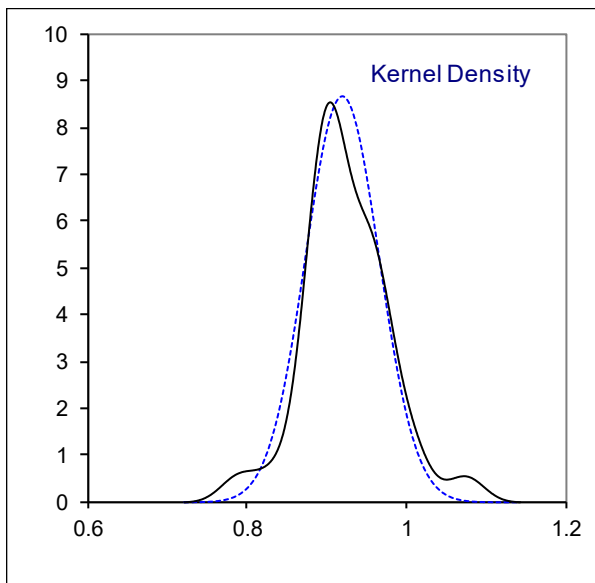
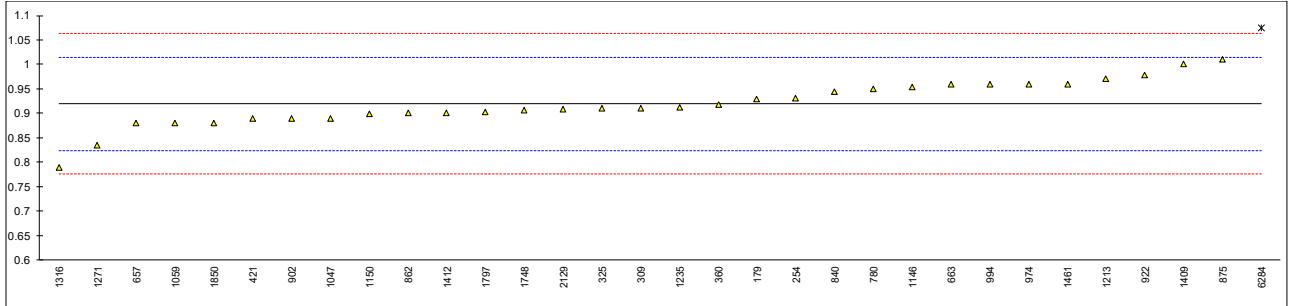
| | |
|-------------------|---------|
| normality | suspect |
| n | 17 |
| outliers | 0 |
| mean (n) | -42.12 |
| st.dev. (n) | 3.257 |
| R(calc.) | 9.12 |
| st.dev.(D5950:14) | 1.607 |
| R(D5950:14) | 4.5 |



Determination of Sulfated Ash on sample #20075; results in %M/M

| lab | method | value | mark | z(targ) | remarks |
|------|---------|--------|---------|---------|---------|
| 178 | | ---- | | ---- | |
| 179 | D874 | 0.929 | | 0.20 | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | | ---- | | ---- | |
| 254 | D874 | 0.93 | | 0.22 | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | D874 | 0.91 | | -0.20 | |
| 325 | D874 | 0.91 | | -0.20 | |
| 329 | | ---- | | ---- | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | | ---- | | ---- | |
| 360 | ISO3987 | 0.917 | | -0.05 | |
| 398 | | ---- | | ---- | |
| 421 | ISO3987 | 0.89 | | -0.62 | |
| 432 | | ---- | | ---- | |
| 496 | | ---- | | ---- | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D874 | 0.88 | | -0.83 | |
| 663 | D874 | 0.96 | | 0.85 | |
| 780 | D874 | 0.95 | | 0.64 | |
| 823 | | ---- | | ---- | |
| 840 | D874 | 0.944 | | 0.52 | |
| 862 | D874 | 0.900 | | -0.41 | |
| 875 | D874 | 1.01 | | 1.90 | |
| 902 | D874 | 0.89 | | -0.62 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D874 | 0.978 | | 1.23 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D874 | 0.96 | | 0.85 | |
| 994 | D874 | 0.96 | | 0.85 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | ISO3987 | 0.89 | | -0.62 | |
| 1059 | ISO3987 | 0.88 | | -0.83 | |
| 1091 | | ---- | | ---- | |
| 1146 | D874 | 0.954 | | 0.73 | |
| 1150 | ISO3987 | 0.8979 | | -0.45 | |
| 1173 | | ---- | | ---- | |
| 1213 | D874 | 0.97 | | 1.06 | |
| 1235 | ISO3987 | 0.9112 | | -0.17 | |
| 1271 | ISO3987 | 0.835 | | -1.77 | |
| 1316 | D874 | 0.79 | | -2.72 | |
| 1320 | | ---- | | ---- | |
| 1409 | D874 | 1.00 | | 1.69 | |
| 1412 | D874 | 0.90 | | -0.41 | |
| 1438 | | ---- | | ---- | |
| 1461 | ISO3987 | 0.96 | | 0.85 | |
| 1510 | | ---- | | ---- | |
| 1564 | | ---- | | ---- | |
| 1748 | D874 | 0.9056 | | -0.29 | |
| 1797 | ISO3987 | 0.903 | | -0.35 | |
| 1850 | ISO3987 | 0.88 | | -0.83 | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | D874 | 0.9077 | | -0.25 | |
| 6016 | | ---- | | ---- | |
| 6032 | | ---- | | ---- | |
| 6183 | | ---- | | ---- | |
| 6197 | | ---- | | ---- | |
| 6253 | | ---- | | ---- | |
| 6284 | D874 | 1.074 | R(0.01) | 3.25 | |
| 6310 | | ---- | | ---- | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

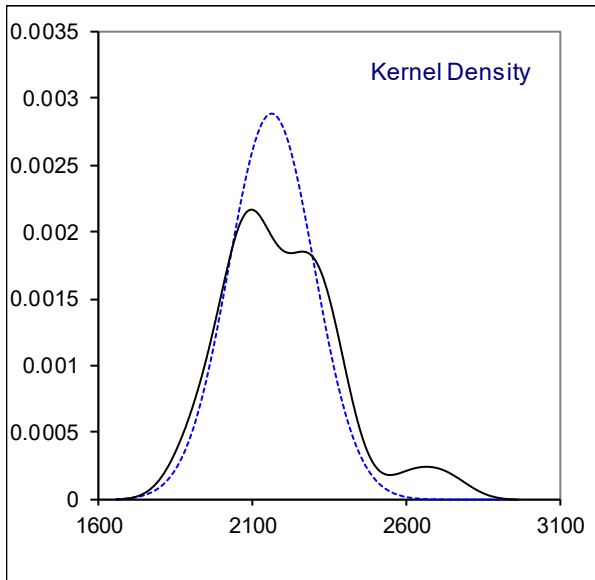
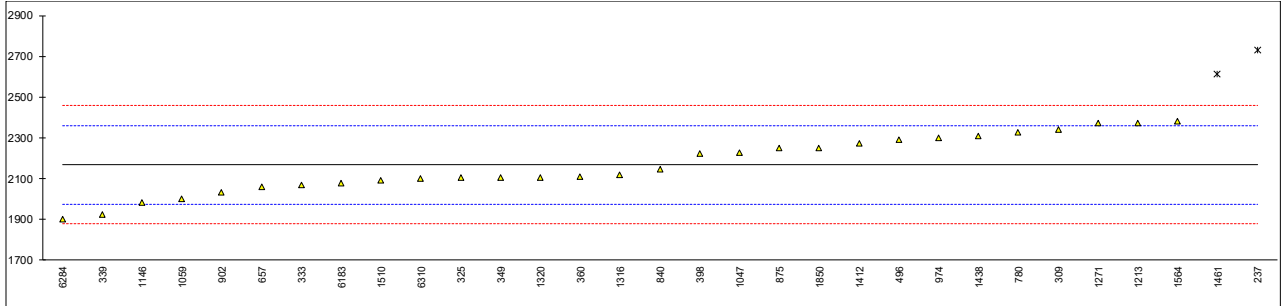
| | |
|-------------------|---------|
| normality | suspect |
| n | 31 |
| outliers | 1 |
| mean (n) | 0.919 |
| st.dev. (n) | 0.0460 |
| R(calc.) | 0.129 |
| st.dev.(D874:13a) | 0.0476 |
| R(D874:13a) | 0.133 |



Determination of Sulfur on sample #20075; results in mg/kg

| lab | method | value | mark | z(targ) | remarks |
|------|--------------|---------|-----------|---------|----------------------------|
| 178 | | ---- | | ---- | |
| 179 | | ---- | | ---- | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | D4294 | 2730 | R(0.01) | 5.82 | |
| 254 | | ---- | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | D2622 | 2340 | | 1.79 | |
| 325 | D5185 | 2105 | | -0.64 | |
| 329 | | ---- | | ---- | |
| 333 | D4294 | 2070 | | -1.00 | |
| 339 | INH-050 | 1925 | | -2.49 | |
| 349 | D2622 | 2105 | | -0.64 | |
| 360 | D4294 | 2110 | | -0.58 | |
| 398 | ISO8754 | 2220 | | 0.55 | |
| 421 | | ---- | | ---- | |
| 432 | | ---- | | ---- | |
| 496 | D4294 | 2290 | | 1.28 | |
| 614 | | ---- | | ---- | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D4294 | 2060 | | -1.10 | |
| 663 | | ---- | | ---- | |
| 780 | D4294 | 2325 | | 1.64 | |
| 823 | | ---- | | ---- | |
| 840 | D5453 | 2144.7 | | -0.23 | |
| 862 | | ---- | | ---- | |
| 875 | D4294 | 2250 | | 0.86 | |
| 902 | D4294 | 2030 | | -1.41 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | | ---- | | ---- | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | D4294 | 2300 | | 1.38 | |
| 994 | | ---- | | ---- | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | ISO8754 | 2228 | | 0.64 | |
| 1059 | ISO14596Mod. | 2000 | | -1.72 | |
| 1091 | | ---- | | ---- | |
| 1146 | In house | 1980 | C | -1.93 | first reported 0.198 mg/kg |
| 1150 | | ---- | | ---- | |
| 1173 | | ---- | | ---- | |
| 1213 | D4294 | 2371 | | 2.11 | |
| 1235 | | ---- | | ---- | |
| 1271 | D4294 | 2370 | | 2.10 | |
| 1316 | D7751 | 2120 | | -0.48 | |
| 1320 | ISO8754 | 2106 | C | -0.62 | first reported 2610 |
| 1409 | | ---- | | ---- | |
| 1412 | D4294 | 2273 | | 1.10 | |
| 1438 | | 2310 | | 1.48 | |
| 1461 | ISO8754 | 2612 | C,R(0.01) | 4.60 | first reported 2587 |
| 1510 | D4294 | 2090 | | -0.79 | |
| 1564 | D5453 | 2380 | | 2.21 | |
| 1748 | | ---- | | ---- | |
| 1797 | | ---- | | ---- | |
| 1850 | ISO8754 | 2250 | | 0.86 | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | | ---- | | ---- | |
| 6016 | | ---- | | ---- | |
| 6032 | | ---- | | ---- | |
| 6183 | D2622 | 2075.27 | | -0.94 | |
| 6197 | | ---- | | ---- | |
| 6253 | | ---- | | ---- | |
| 6284 | D5453 | 1900.2 | | -2.75 | |
| 6310 | D7751 | 2100 | | -0.69 | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

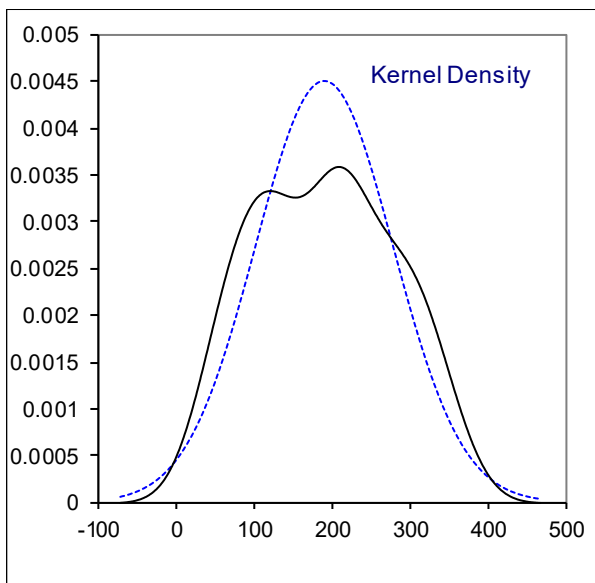
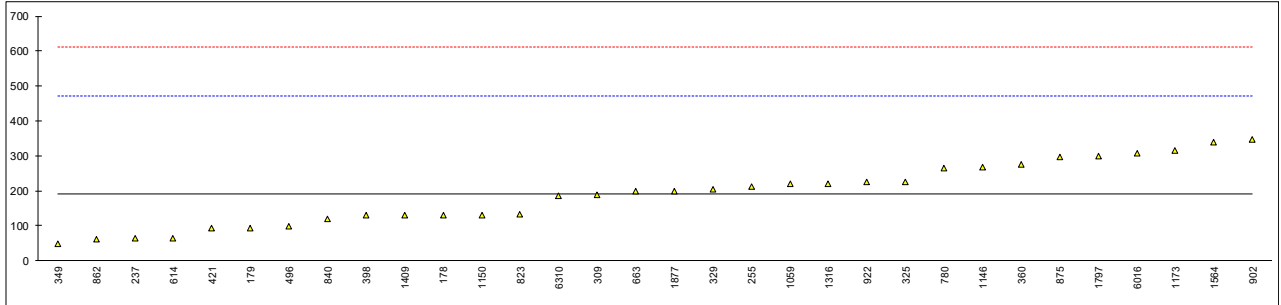
normality OK
n 29
outliers 2
mean (n) 2166.5
st.dev. (n) 138.40
R(calc.) 387.5
st.dev.(D4294:16e1) 96.82
R(D4294:16e1) 271.1



Determination of Water on sample #20075; results in mg/kg

| lab | method | value | mark | z(targ) | remarks |
|------|----------|-------|------|---------|-----------------------------|
| 178 | D6304-C | 131 | | -0.42 | |
| 179 | D6304-C | 94 | | -0.68 | |
| 211 | | ---- | | ---- | |
| 219 | | ---- | | ---- | |
| 237 | D6304-C | 62.8 | | -0.91 | |
| 254 | | ---- | | ---- | |
| 255 | D6304-A | 213 | | 0.16 | |
| 257 | | ---- | | ---- | |
| 309 | D6304-C | 188 | | -0.02 | |
| 325 | D6304-C | 225 | | 0.25 | |
| 329 | D6304-C | 203 | | 0.09 | |
| 333 | | ---- | | ---- | |
| 339 | | ---- | | ---- | |
| 349 | D6304-C | 48 | | -1.01 | |
| 360 | D6304-C | 275.2 | | 0.60 | |
| 398 | ISO12937 | 130 | | -0.43 | |
| 421 | D6304-C | 93.03 | | -0.69 | |
| 432 | | ---- | | ---- | |
| 496 | D6304-C | 99 | | -0.65 | |
| 614 | D6304-C | 63 | | -0.90 | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | D6304-C | <10 | | ---- | |
| 663 | D6304-C | 198.3 | | 0.06 | |
| 780 | D6304-C | 264.7 | | 0.53 | |
| 823 | D6304-C | 132 | | -0.41 | |
| 840 | D6304-C | 120 | | -0.50 | |
| 862 | D6304-C | 62 | | -0.91 | |
| 875 | D6304-A | 297 | | 0.76 | |
| 902 | D6304-C | 348 | | 1.12 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | D6304-A | 224 | | 0.24 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | | ---- | | ---- | |
| 994 | | ---- | | ---- | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | ---- | | ---- | |
| 1059 | D6304-C | 220 | | 0.21 | |
| 1091 | | ---- | | ---- | |
| 1146 | D6304-C | 268 | | 0.55 | |
| 1150 | ISO12937 | 131 | C | -0.42 | first reported 0.1309 % M/M |
| 1173 | In house | 314.0 | | 0.88 | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | | ---- | | ---- | |
| 1316 | D6304-C | 220 | | 0.21 | |
| 1320 | | ---- | | ---- | |
| 1409 | D6304-A | 130 | | -0.43 | |
| 1412 | | ---- | | ---- | |
| 1438 | | ---- | | ---- | |
| 1461 | | ---- | | ---- | |
| 1510 | | ---- | | ---- | |
| 1564 | D6304-C | 339 | | 1.06 | |
| 1748 | | ---- | | ---- | |
| 1797 | D95 | 300 | | 0.78 | |
| 1850 | | ---- | | ---- | |
| 1877 | D6304-C | 200 | | 0.07 | |
| 1969 | | ---- | | ---- | |
| 2129 | | ---- | | ---- | |
| 6016 | | 308 | | 0.84 | |
| 6032 | | ---- | | ---- | |
| 6183 | | ---- | | ---- | |
| 6197 | | ---- | | ---- | |
| 6253 | | ---- | | ---- | |
| 6284 | | ---- | | ---- | |
| 6310 | D6304-C | 185 | | -0.04 | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

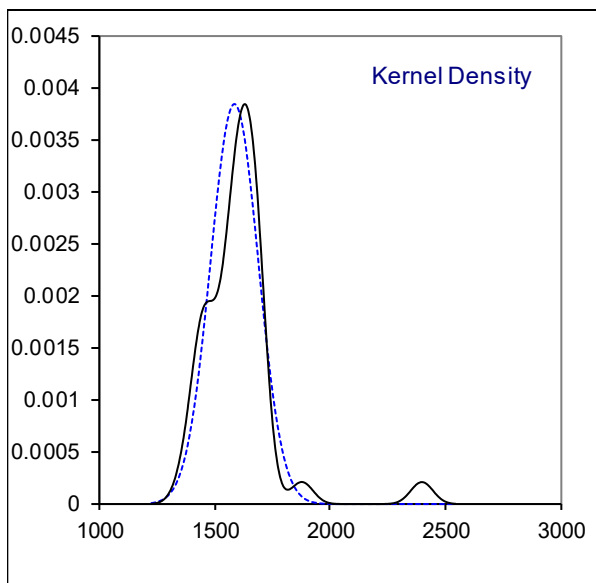
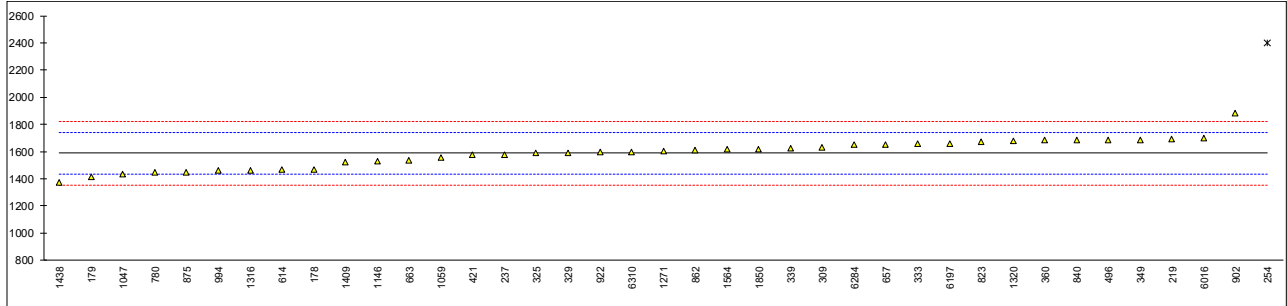
| | |
|---------------------|----------|
| normality | OK |
| n | 32 |
| outliers | 0 |
| mean (n) | 190.188 |
| st.dev. (n) | 88.3899 |
| R(calc.) | 247.492 |
| st.dev.(D6304:16e1) | 140.6130 |
| R(D6304:16e1) | 393.716 |



Determination of Calcium as Ca on sample #20075; results in mg/kg

| lab | method | value | mark | z(targ) | remarks |
|------|--------|-----------|-----------|---------|-------------------------|
| 178 | | 1469 | | -1.53 | |
| 179 | | 1416 | | -2.21 | |
| 211 | | ---- | | ---- | |
| 219 | | 1689 | | 1.31 | |
| 237 | | 1576 | | -0.15 | |
| 254 | | 2400.58 | C,R(0.01) | 10.48 | first reported 1897.165 |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | 1632 | | 0.58 | |
| 325 | | 1589 | | 0.02 | |
| 329 | | 1592 | | 0.06 | |
| 333 | | 1655 | | 0.87 | |
| 339 | | 1623 | | 0.46 | |
| 349 | | 1686 | | 1.27 | |
| 360 | | 1683 | | 1.23 | |
| 398 | | ---- | | ---- | |
| 421 | | 1575 | | -0.16 | |
| 432 | | ---- | | ---- | |
| 496 | | 1685 | | 1.26 | |
| 614 | | 1465 | | -1.58 | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | | 1653 | | 0.85 | |
| 663 | | 1536.95 | | -0.65 | |
| 780 | | 1445 | | -1.83 | |
| 823 | | 1669 | | 1.05 | |
| 840 | | 1685 | | 1.26 | |
| 862 | | 1609 | | 0.28 | |
| 875 | | 1450 | C | -1.77 | first reported 2380 |
| 902 | | 1880 | | 3.77 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | | 1597 | | 0.12 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | | ---- | | ---- | |
| 994 | | 1460 | | -1.64 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | 1433.7 | | -1.98 | |
| 1059 | | 1557 | | -0.39 | |
| 1091 | | ---- | | ---- | |
| 1146 | | 1531 | | -0.73 | |
| 1150 | | ---- | | ---- | |
| 1173 | | ---- | | ---- | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | | 1601 | | 0.18 | |
| 1316 | | 1460 | | -1.64 | |
| 1320 | | 1679 | | 1.18 | |
| 1409 | | 1519 | | -0.88 | |
| 1412 | | ---- | | ---- | |
| 1438 | | 1372 | C | -2.78 | first reported 1310 |
| 1461 | | ---- | | ---- | |
| 1510 | | ---- | | ---- | |
| 1564 | | 1614 | | 0.34 | |
| 1748 | | ---- | | ---- | |
| 1797 | | ---- | | ---- | |
| 1850 | | 1620 | | 0.42 | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | | ---- | | ---- | |
| 6016 | | 1700 | | 1.45 | |
| 6032 | | ---- | | ---- | |
| 6183 | | ---- | | ---- | |
| 6197 | | 1661 | | 0.95 | |
| 6253 | | ---- | | ---- | |
| 6284 | | 1652.1667 | | 0.84 | |
| 6310 | | 1600 | | 0.16 | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

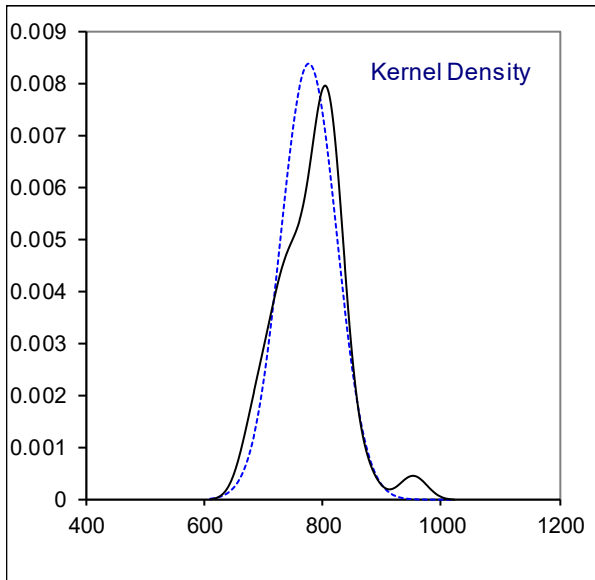
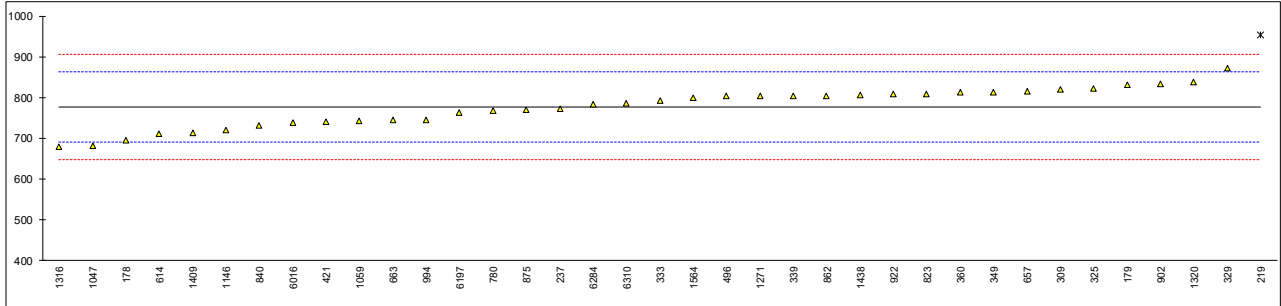
| | |
|-------------------|---------|
| normality | OK |
| n | 38 |
| outliers | 1 |
| mean (n) | 1587.36 |
| st.dev. (n) | 103.669 |
| R(calc.) | 290.27 |
| st.dev.(D5185:18) | 77.591 |
| R(D5185:18) | 217.26 |



Determination of Phosphorus as P on sample #20075; results in mg/kg

| lab | method | value | mark | z(targ) | remarks |
|------|--------|--------|---------|---------|---------------------|
| 178 | | 696 | | -1.89 | |
| 179 | | 832 | | 1.28 | |
| 211 | | ---- | | ---- | |
| 219 | | 954 | R(0.05) | 4.13 | |
| 237 | | 772.7 | | -0.10 | |
| 254 | | ---- | | ---- | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | 819.9 | | 1.00 | |
| 325 | | 821 | | 1.03 | |
| 329 | | 872 | | 2.22 | |
| 333 | | 792 | | 0.35 | |
| 339 | | 804 | | 0.63 | |
| 349 | | 813 | | 0.84 | |
| 360 | | 813 | | 0.84 | |
| 398 | | ---- | | ---- | |
| 421 | | 740 | | -0.87 | |
| 432 | | ---- | | ---- | |
| 496 | | 803.1 | | 0.61 | |
| 614 | | 711.3 | | -1.54 | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | | 816 | | 0.91 | |
| 663 | | 744.34 | | -0.76 | |
| 780 | | 767 | | -0.24 | |
| 823 | | 809 | | 0.75 | |
| 840 | | 731 | | -1.08 | |
| 862 | | 805 | | 0.65 | |
| 875 | | 770 | C | -0.17 | first reported 1140 |
| 902 | | 834 | | 1.33 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | | 808 | | 0.72 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | | ---- | | ---- | |
| 994 | | 746 | | -0.73 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | 680.4 | | -2.26 | |
| 1059 | | 743 | | -0.80 | |
| 1091 | | ---- | | ---- | |
| 1146 | | 719.6 | | -1.34 | |
| 1150 | | ---- | | ---- | |
| 1173 | | ---- | | ---- | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | | 803.5 | | 0.62 | |
| 1316 | | 680 | | -2.27 | |
| 1320 | | 838 | | 1.42 | |
| 1409 | | 713 | | -1.50 | |
| 1412 | | ---- | | ---- | |
| 1438 | | 806 | C | 0.68 | first reported 916 |
| 1461 | | ---- | | ---- | |
| 1510 | | ---- | | ---- | |
| 1564 | | 800 | | 0.54 | |
| 1748 | | ---- | | ---- | |
| 1797 | | ---- | | ---- | |
| 1850 | | ---- | | ---- | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | | ---- | | ---- | |
| 6016 | | 738 | | -0.91 | |
| 6032 | | ---- | | ---- | |
| 6183 | | ---- | | ---- | |
| 6197 | | 764 | | -0.31 | |
| 6253 | | ---- | | ---- | |
| 6284 | | 784.15 | | 0.17 | |
| 6310 | | 785 | | 0.18 | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

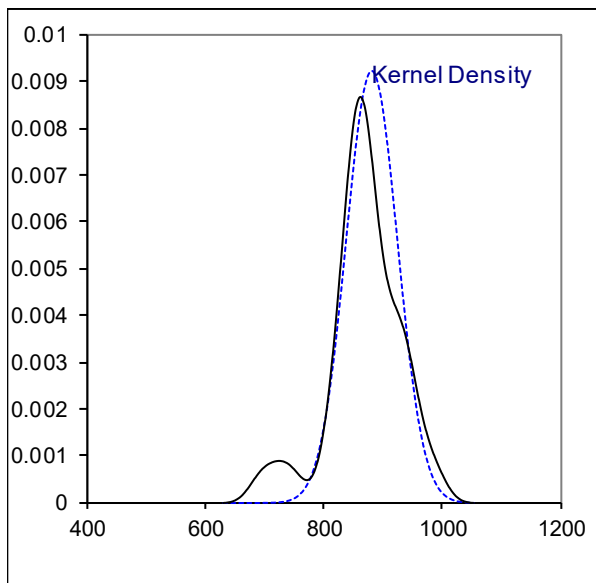
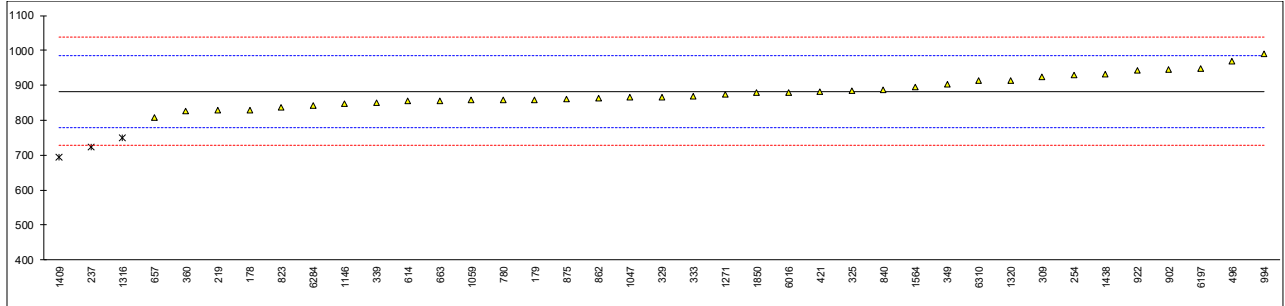
| | |
|-------------------|--------|
| normality | OK |
| n | 36 |
| outliers | 1 |
| mean (n) | 777.08 |
| st.dev. (n) | 47.520 |
| R(calc.) | 133.06 |
| st.dev.(D5185:18) | 42.810 |
| R(D5185:18) | 119.87 |



Determination of Zinc as Zn on sample #20075; results in mg/kg

| lab | method | value | mark | z(target) | remarks |
|------|--------|---------|---------|-----------|----------------------|
| 178 | | 828 | | -1.06 | |
| 179 | | 859 | | -0.46 | |
| 211 | | ---- | | ---- | |
| 219 | | 828 | | -1.06 | |
| 237 | | 724 | R(0.01) | -3.07 | |
| 254 | | 929.458 | | 0.91 | |
| 255 | | ---- | | ---- | |
| 257 | | ---- | | ---- | |
| 309 | | 923.5 | | 0.80 | |
| 325 | | 885 | | 0.05 | |
| 329 | | 867 | | -0.30 | |
| 333 | | 868 | | -0.28 | |
| 339 | | 851 | | -0.61 | |
| 349 | | 904 | | 0.42 | |
| 360 | | 826 | | -1.10 | |
| 398 | | ---- | | ---- | |
| 421 | | 881 | | -0.03 | |
| 432 | | ---- | | ---- | |
| 496 | | 968.7 | | 1.67 | |
| 614 | | 854.3 | | -0.55 | |
| 621 | | ---- | | ---- | |
| 633 | | ---- | | ---- | |
| 634 | | ---- | | ---- | |
| 657 | | 807 | | -1.46 | |
| 663 | | 855.66 | | -0.52 | |
| 780 | | 859 | | -0.46 | |
| 823 | | 836 | | -0.90 | |
| 840 | | 888 | | 0.11 | |
| 862 | | 864 | | -0.36 | |
| 875 | | 860 | C | -0.44 | first reported 1300 |
| 902 | | 945 | | 1.21 | |
| 912 | | ---- | | ---- | |
| 913 | | ---- | | ---- | |
| 922 | | 943 | | 1.17 | |
| 962 | | ---- | | ---- | |
| 963 | | ---- | | ---- | |
| 974 | | ---- | | ---- | |
| 994 | | 991 | | 2.11 | |
| 1011 | | ---- | | ---- | |
| 1017 | | ---- | | ---- | |
| 1047 | | 865 | C | -0.34 | first reported 767.1 |
| 1059 | | 857 | | -0.49 | |
| 1091 | | ---- | | ---- | |
| 1146 | | 848.0 | | -0.67 | |
| 1150 | | ---- | | ---- | |
| 1173 | | ---- | | ---- | |
| 1213 | | ---- | | ---- | |
| 1235 | | ---- | | ---- | |
| 1271 | | 875 | | -0.15 | |
| 1316 | | 750 | R(0.01) | -2.57 | |
| 1320 | | 914 | | 0.61 | |
| 1409 | | 695 | R(0.01) | -3.64 | |
| 1412 | | ---- | | ---- | |
| 1438 | | 933 | C | 0.98 | first reported 1037 |
| 1461 | | ---- | | ---- | |
| 1510 | | ---- | | ---- | |
| 1564 | | 894 | | 0.22 | |
| 1748 | | ---- | | ---- | |
| 1797 | | ---- | | ---- | |
| 1850 | | 880 | | -0.05 | |
| 1877 | | ---- | | ---- | |
| 1969 | | ---- | | ---- | |
| 2129 | | ---- | | ---- | |
| 6016 | | 880 | | -0.05 | |
| 6032 | | ---- | | ---- | |
| 6183 | | ---- | | ---- | |
| 6197 | | 947 | | 1.25 | |
| 6253 | | ---- | | ---- | |
| 6284 | | 841.7 | | -0.79 | |
| 6310 | | 913 | | 0.59 | |
| 6317 | | ---- | | ---- | |
| 6320 | | ---- | | ---- | |
| 6324 | | ---- | | ---- | |

| | |
|-------------------|--------|
| normality | OK |
| n | 36 |
| outliers | 3 |
| mean (n) | 882.48 |
| st.dev. (n) | 43.329 |
| R(calc.) | 121.32 |
| st.dev.(D5185:18) | 51.546 |
| R(D5185:18) | 144.33 |



APPENDIX 2**Number of participants per country**

| | |
|-----------------------------------|------------------------------------|
| 1 lab in AUSTRALIA | 2 labs in PAKISTAN |
| 1 lab in AUSTRIA | 1 lab in PERU |
| 2 labs in AZERBAIJAN | 2 labs in PHILIPPINES |
| 7 labs in BELGIUM | 2 labs in POLAND |
| 1 lab in BOSNIA and HERZEGOVINA | 1 lab in PORTUGAL |
| 3 labs in BULGARIA | 1 lab in ROMANIA |
| 1 lab in CHINA, People's Republic | 2 labs in RUSSIAN FEDERATION |
| 1 lab in CROATIA | 2 labs in SAUDI ARABIA |
| 1 lab in CZECH REPUBLIC | 2 labs in SINGAPORE |
| 2 labs in FRANCE | 1 lab in SLOVAKIA |
| 2 labs in GERMANY | 1 lab in SLOVENIA |
| 2 labs in INDIA | 1 lab in SOUTH KOREA |
| 1 lab in INDONESIA | 2 labs in SPAIN |
| 1 lab in ISRAEL | 1 lab in SWEDEN |
| 1 lab in ITALY | 3 labs in TANZANIA |
| 1 lab in JORDAN | 1 lab in THAILAND |
| 1 lab in KAZAKHSTAN | 1 lab in TUNISIA |
| 1 lab in KENYA | 1 lab in TURKEY |
| 3 labs in MOROCCO | 1 lab in UNITED ARAB EMIRATES |
| 2 labs in NETHERLANDS | 4 labs in UNITED KINGDOM |
| 1 lab in NIGERIA | 2 labs in UNITED STATES OF AMERICA |
| 1 lab in OMAN | 2 labs in VIETNAM |

APPENDIX 3

Abbreviations

| | |
|----------|--|
| C | = final test result after checking of first reported suspect test result |
| D(0.01) | = outlier in Dixon's outlier test |
| D(0.05) | = straggler in Dixon's outlier test |
| G(0.01) | = outlier in Grubbs' outlier test |
| G(0.05) | = straggler in Grubbs' outlier test |
| DG(0.01) | = outlier in Double Grubbs' outlier test |
| DG(0.05) | = straggler in Double Grubbs' outlier test |
| R(0.01) | = outlier in Rosner's outlier test |
| R(0.05) | = straggler in Rosner's outlier test |
| E | = probably an error in calculations |
| ex | = test result excluded from the statistical evaluation |
| W | = test result withdrawn on request of participant |
| fr. | = first reported |
| n.a. | = not applicable |
| n.e. | = not evaluated |
| SDS | = Safety Data Sheet |

Literature

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- 2 ASTM E178:89
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- 12 J.N. Miller, Analyst, 118, 455, (1993)
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